

Multiple-domain, finite-difference solutions for ocean wave-structure interaction

Robert W. Read Harry B. Bingham

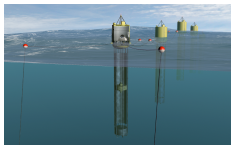
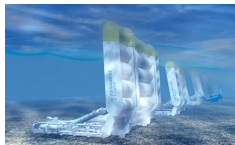
Department of Mechanical Engineering
Technical University of Denmark

10th Symposium on Overset Composite Grids
and Solution Technology
September 23, 2010

Outline

- 1 Background
 - Motivation
 - The problem
 - Aims
- 2 Solution strategy
 - Spatial solution
 - Temporal evolution
 - Numerical framework
- 3 Linear results
 - Standing wave
 - Heaving cylinder
- 4 Summary

Electricity from ocean waves



- Urgent need to deploy renewable energy technologies
- Ocean wave energy can make significant contribution to mix
- Young industry developing many different design concepts
- Practical computational tools required

Modelling water waves

Flow characteristics

- High Reynolds numbers: $> 10^7$
- Incompressible fluid
- Internal flow is irrotational
- Viscosity significant at walls and during wave breaking

Possible simulation approaches

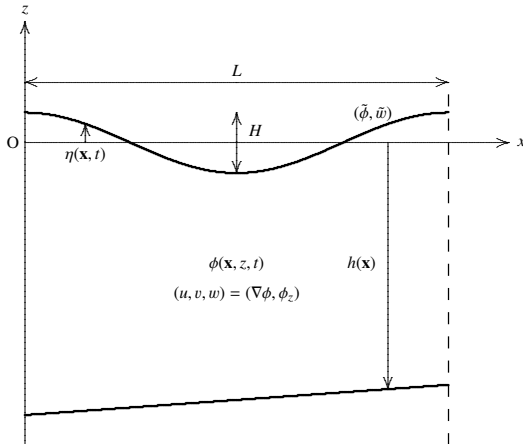
- 1 Direct solution of Navier-Stokes equations
- 2 Inviscid Euler equations
- 3 Boussinesq-type formulations

The potential flow approach

Our strategy

- Assume potential flow
- Separate inclusion of friction and wave breaking effects
- Velocity field is gradient of scalar function: velocity potential
- Implies flow is irrotational and thus inviscid and laminar
- No boundary layers or turbulence
- Fluid assumed incompressible

The non-linear wave problem



Governing equations

Bulk fluid

Laplace's equation: $\nabla^2 \phi + \partial_{zz} \phi = 0$ where $-h \leq z < \eta$

Boundary conditions

1 Free surface

- Kinematic: $\partial_t \eta = \tilde{w} (1 + \nabla \eta \cdot \nabla \eta) - \nabla \tilde{\phi} \cdot \nabla \eta$
- Dynamic: $\partial_t \tilde{\phi} = -g\eta - 1/2 \left(\nabla \tilde{\phi} \cdot \nabla \tilde{\phi} - \tilde{w}^2 (1 + \nabla \eta \cdot \nabla \eta) \right)$

2 Solid surface: $(\mathbf{n}, n_z) \cdot (\nabla, \partial_z) \phi = 0$ where $(\mathbf{x}, z) \in \partial\Omega$

The linear formulation

The assumption

The wave elevation is small compared to the wavelength and the free surface velocity is thus vertical.

Reduced equations

- 1 Laplace's equation: $\nabla^2 \phi + \partial_{zz} \phi = 0$ where $-h \leq z < \eta$
- 2 Free surface
 - Kinematic: $\partial_t \eta = \tilde{w}$
 - Dynamic: $\partial_t \tilde{\phi} = -g\eta$
- 3 Solid surface: $(\mathbf{n}, n_z) \cdot (\nabla, \partial_z) \phi = 0$ where $(\mathbf{x}, z) \in \partial\Omega$

Modelling objectives

Overall

- Simulate fully non-linear wave-body interaction

Preliminary

- Computational tool describing linear case
- Variable depth and complex body geometries

Immediate

- Extend single-block wave model to multiple curvilinear grids

Today's talk: Linear multi-block solutions for wave-body interaction

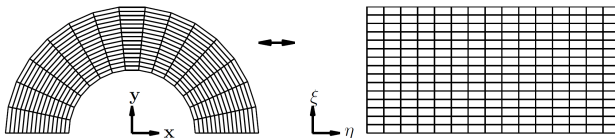
A finite-difference approach

- Require method to identify velocity potential at every grid point
- Represent spatial governing equations in finite-difference form
- Transformations between physical and computational space
- Include interpolation between blocks
- Construct multi-block linear system and solve

Boundary conditions

- Dirichlet condition applied at free-surface points
- Neumann conditions applied at solid-surface ghost points
- Conditions enforced using one of two approaches:
 - 1 off-centred schemes, single ghost layer at solid surface
 - 2 centred schemes, multiple ghost layers and extrapolation

Curvilinear transformations



- Mappings: $[\eta(x, y), \zeta(x, y)]$ and $[x(\eta, \zeta), y(\eta, \zeta)]$
- Partial derivatives in two spaces related by:

$$\partial_x = \zeta_x \partial_\zeta + \eta_x \partial_\eta, \quad \partial_y = \zeta_y \partial_\zeta + \eta_y \partial_\eta, \quad \text{etc.}$$

- Express derivatives as operations in computational space:

$$\partial_x = \frac{1}{J} (y_\eta \partial_\zeta - y_\zeta \partial_\eta) \quad \text{where} \quad J = x_\zeta y_\eta - x_\eta y_\zeta, \quad \text{etc.}$$

A Runge-Kutta approach

- Advance using classical fourth-order Runge-Kutta method

$$\underbrace{\frac{d}{dt} \begin{bmatrix} \eta \\ \tilde{\phi} \end{bmatrix}}_y = \underbrace{\begin{bmatrix} \partial \tilde{\phi} / \partial z \\ -g\eta \end{bmatrix}}_{f(t,y)}, \quad y_{n+1} = y_n + \frac{\delta t}{6} (k_1 + 2k_2 + 2k_3 + k_4)$$

- Time step determination using a Courant number of 0.5

$$\text{CFL condition: } u \frac{\Delta t}{\Delta x} \leq C \quad \text{In this case: } \frac{\delta t / T}{\delta x / \lambda} = 0.5$$

Software

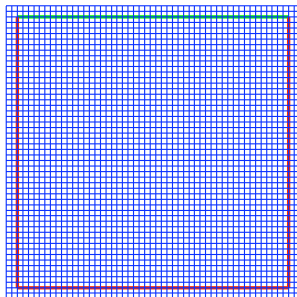
Matlab

- Straightforward implementation, debugging, and testing
- Can maintain total flexibility in spatial order of accuracy

Overture

- Code framework to solve pde's on multiple curved blocks
- C++ libraries provide functionality with low-level control
- Powerful grid generation and parallel processing capabilities
- Multiple solvers, but limited to fourth-order spatially

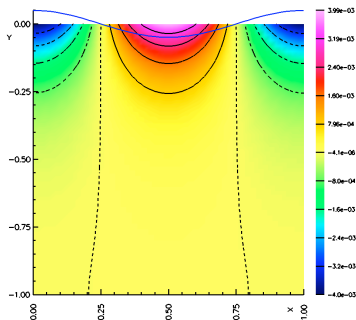
Overture implementation



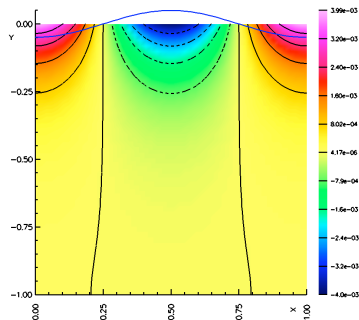
- Unit square, 50 by 50 points
- Sinusoidal surface, $\lambda = 1$ m
- Fourth-order schemes
- Courant number = 0.5

Velocity potential

Potential at time, $t = 0.008$

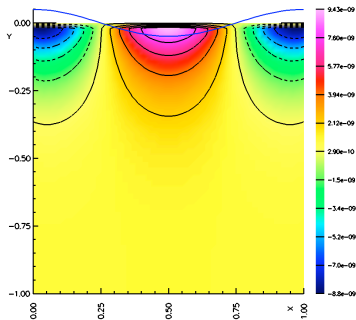


Potential at time, $t = 0.408$

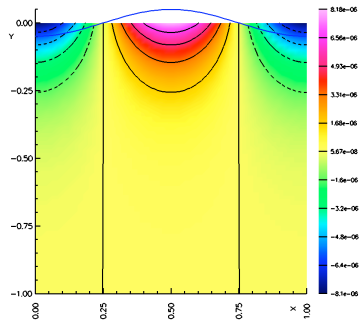


Numerical error

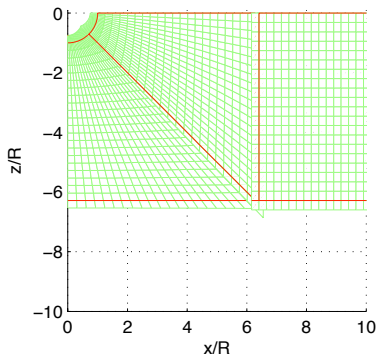
Error at time, $t = 0.008$



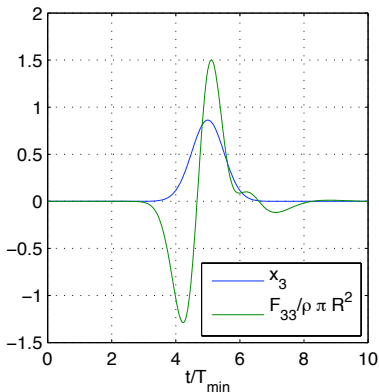
Error at time, $t = 0.408$



Matlab implementation

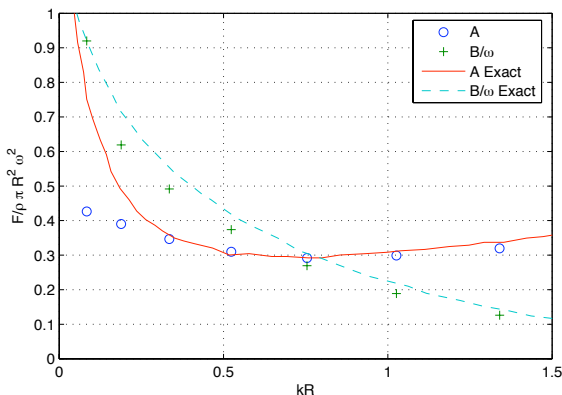


- Vertical flux at cylinder
- Free-surface initially flat



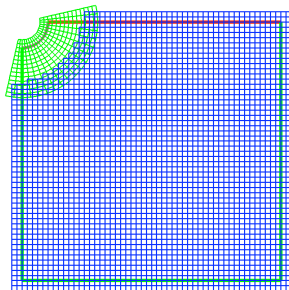
- Sixth-order spatial schemes
- Gaussian displacement profile

Added mass and damping

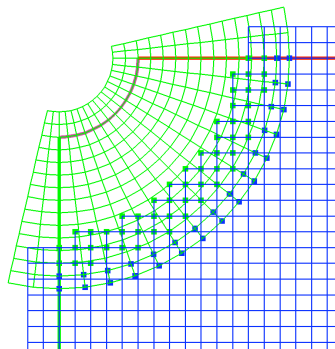


- Good agreement between numerical and analytical solution
- Differences in added mass at long wavelengths expected

Overture implementation



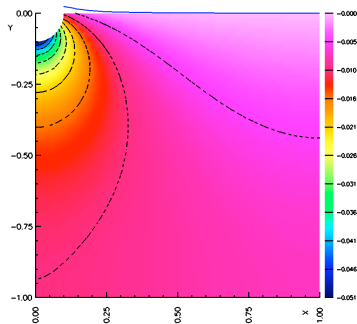
- Vertical flux at cylinder
- Free-surface initially flat



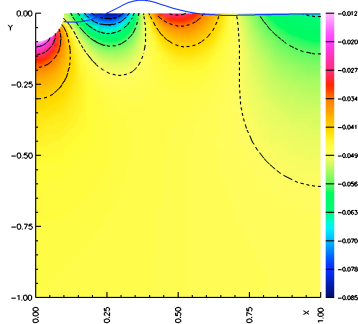
- Fourth-order schemes
- Manufactured solution testing

The velocity potential

Potential at time, $t = 0.113$



Potential at time, $t = 1.019$



Outlook

Accomplishments

- Implemented linear wave models on curvilinear multiblock geometries
- Evaluated added mass and damping of heaving cylinder

Work in progress - Overture

- Evaluate added mass and damping and compare results
- Investigate using arbitrary-order spatial schemes
- Implement iterative solver
- Further investigate grid generation capabilities and extend to 3-d

Acknowledgements

- This work is supported by the Danish Council for Strategic Research through the Structural Design of Wave Energy Devices project.
- We wish to thank Bill Henshaw for his help and guidance using the Overture package.