



RDECOM

10th Overset Composite Grids and Solution Technology Symposium

NASA-Ames Research Center

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CFD/CSD Coupling and Trim of the SMART Rotor



TECHNOLOGY DRIVEN. WARFIGHTER FOCUSED.

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Lift to drag ratio	+ 8%
Maximum blade loading	+24%
Vibratory response	-30%
Detection distance	-50%



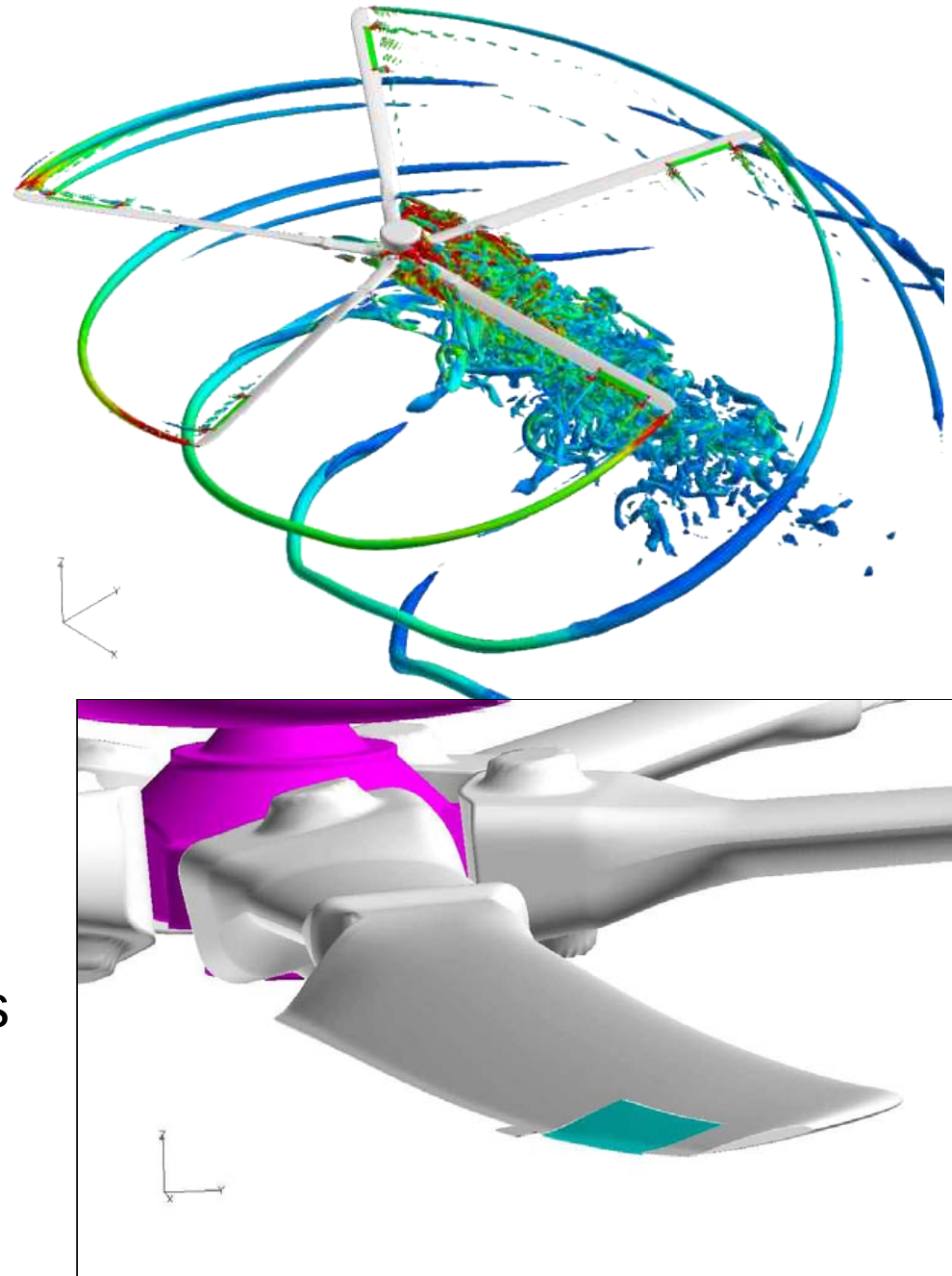
- Army S&T aeromechanics technology objectives
 - Improved rotorcraft characteristics
 - Aeromechanics modeling, accuracy & productivity improvement
- Army rotorcraft CFD
 - Development of CFD software analysis tools
 - HPCMO HI-ARMS Institute / CREATE-AV
 - High performance computing
 - Rotorcraft aerodynamics problems require state-of-the-art high-performance computers
 - Cutting-edge research and application to DoD aircraft
 - Improve design process by complementing existing design methods

- Benefits of performance, vibration, and noise advancements
 - Improved range, payload, speed, maneuverability
 - Improved component life
 - Reduced maintenance
 - Improved community acceptance
 - Decreased acoustic detectability

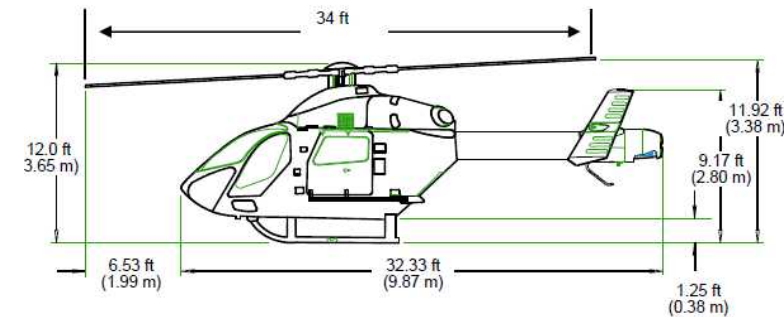
Boeing SMART Rotor (40x80)



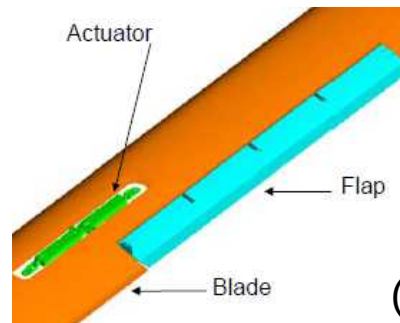
- Unsteady, interactional aerodynamics
- Complex, high-fidelity geometry
- Large range of flow velocities
 - Hover, cruise, maneuver
 - Low subsonic to supersonic
- Disparate length and time scales
 - Rotor, wake, vortices, viscous layers
- Wake modeling
 - Minimize numerical dissipation and convect over long distances
- Turbulence modeling
- Multidisciplinary coupling



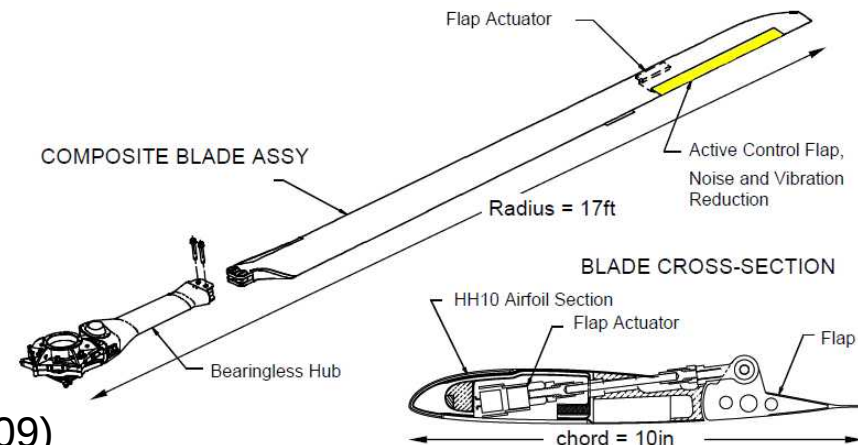
- Boeing Smart Material Actuated Rotor Technology (SMART) rotor
 - Full-scale, 5-bladed, flapped MD900 bearingless rotor
 - 16.9 ft radius, 10 inch chord, parabolic tip
 - 18% span piezoelectric flap (74 - 92% R), 35% chord
 - 0.62 hover tip Mach number
- Objectives to demonstrate reductions in
 - Noise: in-plane, blade-vortex interaction (BVI)
 - Vibration
 - Power: cruise - 123, 155 kts ($\mu = 0.30, 0.38$)



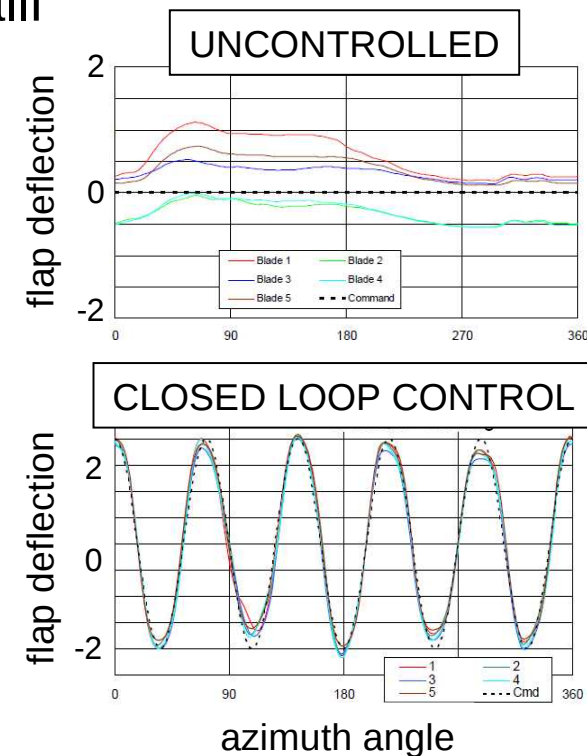
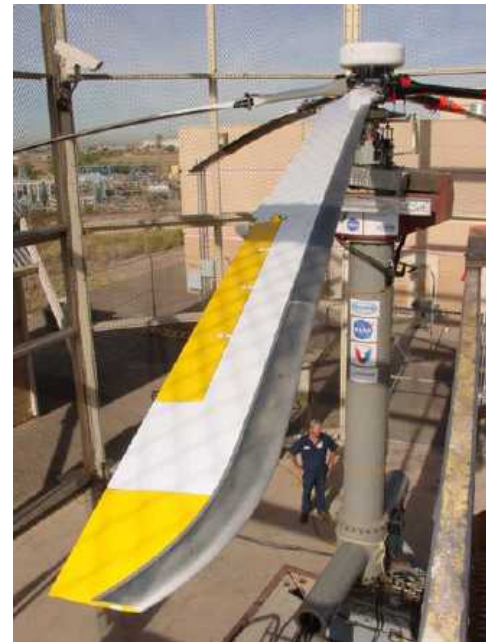
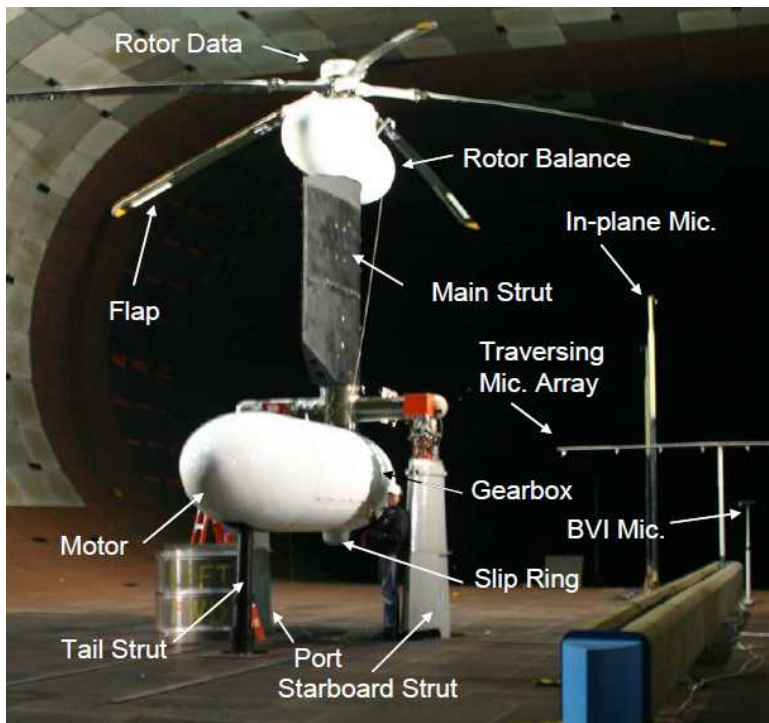
MD900 HELICOPTER



(Straub 2009)



- DARPA/BoeingNASA/Army test in the DoD National Full-Scale Aerodynamic Complex 40- x 80-Ft Wind Tunnel (NASA Ames)
 - Database of blade and pitch link structural loads, control positions, rotor forces and moments, BVI and in-plane microphones ?(no surface pressures)
 - Papers by Straub, Hall, JanikaRam, Sim, and Kottapalli at 2009 AHS Forum



closed loop flap control
(Straub/Hall 2009)

- CAMRAD II

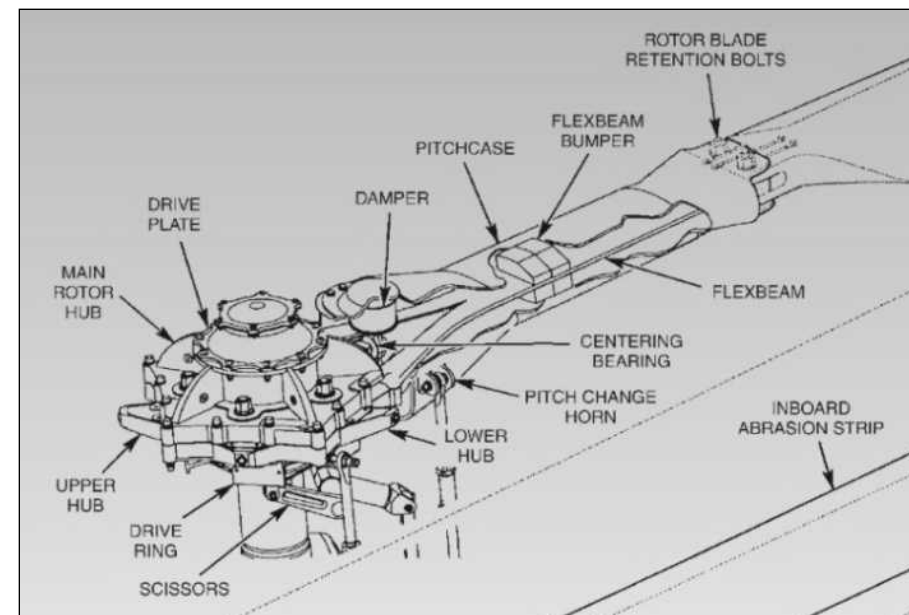
- State-of-the-art multidisciplinary rotorcraft comprehensive analysis (CA) performs structural dynamics and trim
- CFD/CSD coupling replaces CA aerodynamics
- Important to ensure CFD and CSD geometric consistency

- Aerodynamic model

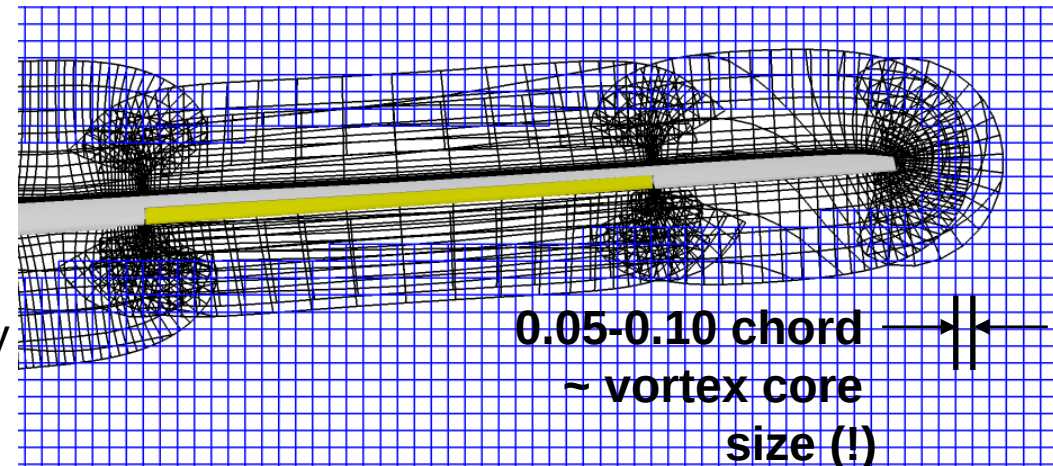
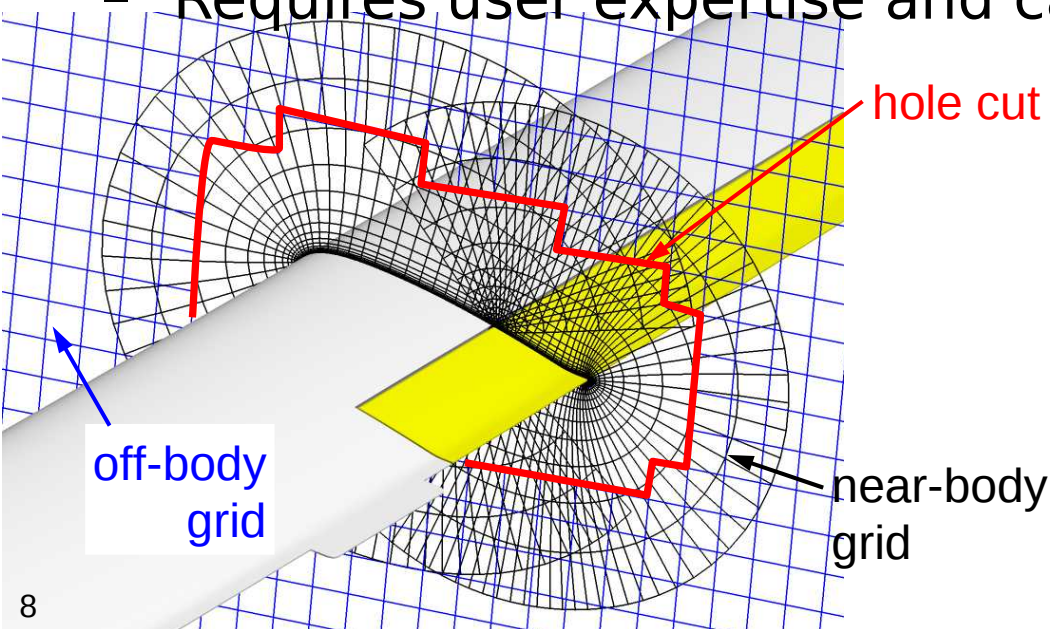
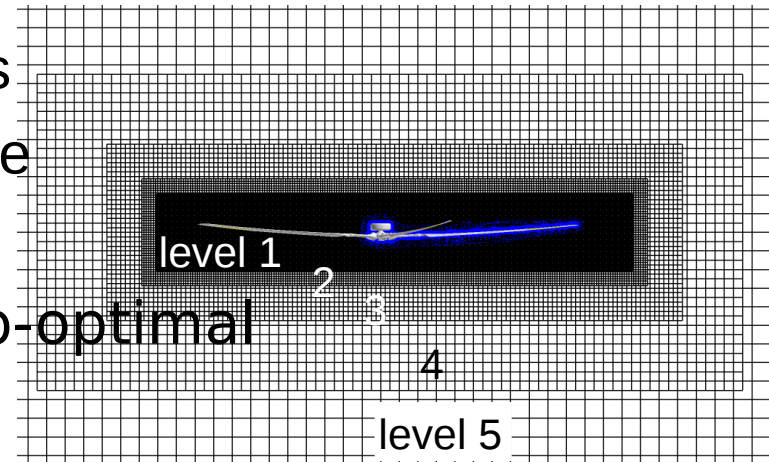
- Blade element lifting-line aerodynamics with airfoil table lookup ($Mach$, α , δ_f)
- 20 aerodynamic panels with continuous flap
- Free wake (CA) or uniform inflow (CFD/CSD)

- Structural model

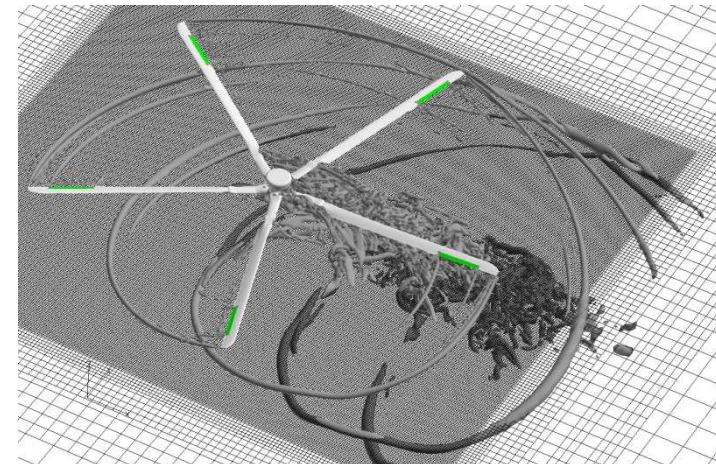
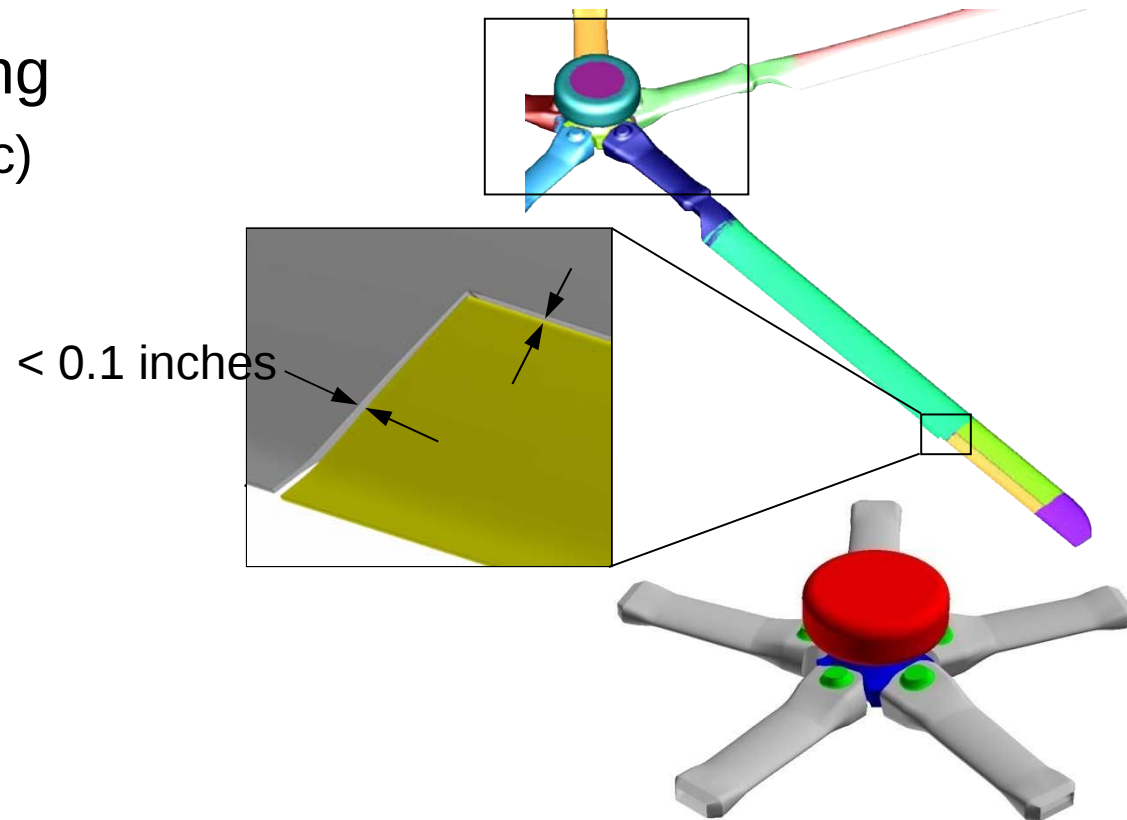
- Boeing SMART rotor properties (NASA/Boeing)
- 10 non-linear beam finite elements:
 - Axial, lead-lag, flap, torsion and DOFs
 - Dual load path blade root (flexbeam/pitchcase)
- *Elastic trailing edge flap* with 5 hinges
- Compliant pitch links
- 18 modes used
- *Numerical conditioning issues*



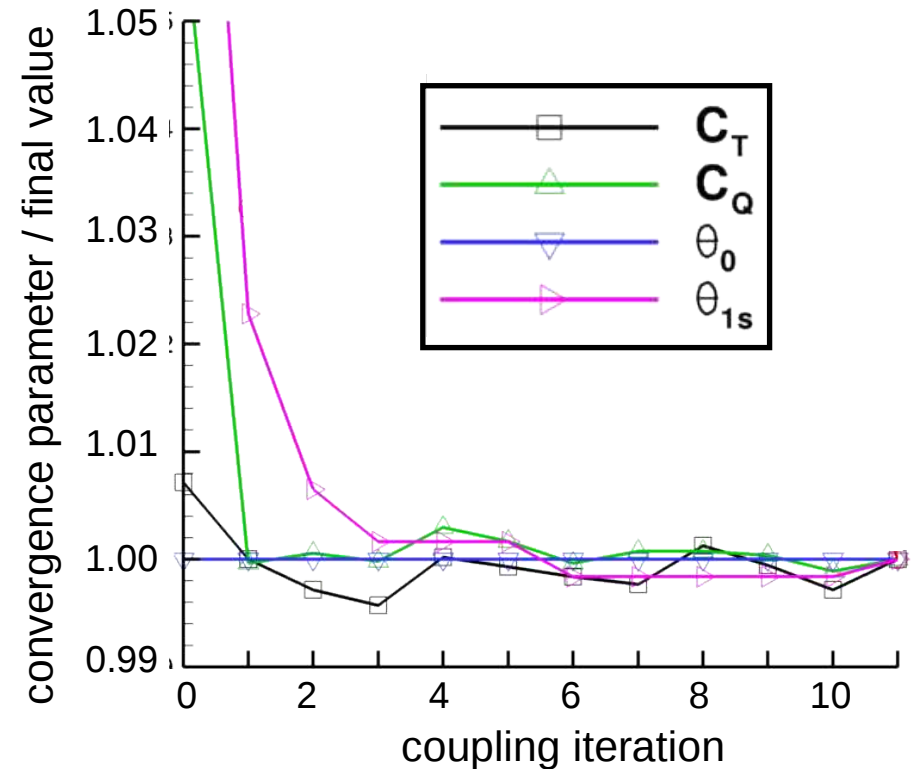
- OVERFLOW 2.0aa (NASA/Army)
 - Near-body, off-body overset grid paradigm
- Body-fitted, stretched curvilinear "near-body" grids
 - Structured grid generation is labor intensive for complex configurations
- Automatic, multi-level, Cartesian "off-body" grids
 - Efficient, accurate, automated, and adaptable
- Subroutine-activated domain connectivity
 - Requires user expertise and can be sub-optimal



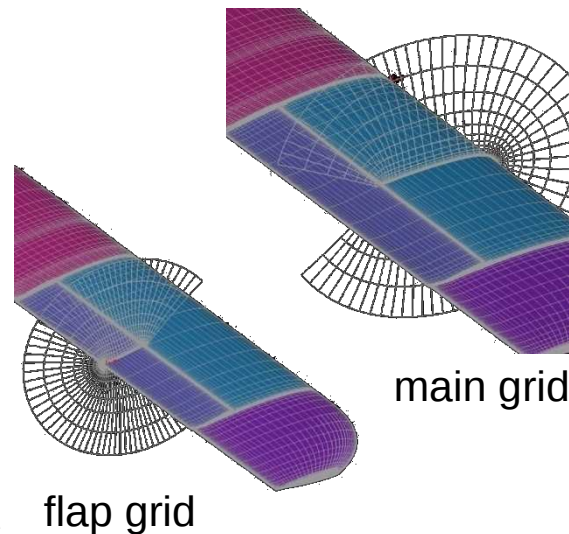
- High-fidelity geometric modeling
 - Pitchcase, blade and flap (elastic)
 - Hub and instrumentation fairing
 - *Discrete flap gaps*
- Grid generation
 - Baseline (coarse) grid
 - 17 million grid points
 - 820,000 points per blade
 - 75% off-body
 - 12% chord wake spacing
 - Fine grid with 66 million points
- Numerical scheme
 - 3rd-order spatial central-difference scheme with matrix dissipation
 - 2nd-order temporal scheme with subiterative dual-time stepping
 - 0.25° time step (RPM?)



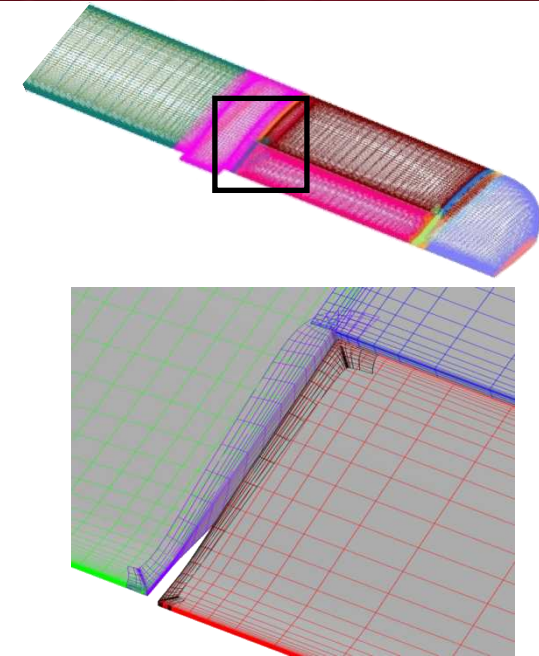
- Loose coupling exchanges periodic forces/moments
- “Dual rotor” concept, main and flap treated as separate “rotors” in CFD
- Modifications for multiple grids per blade
- Convergence on controls, forces/moments, and airloads



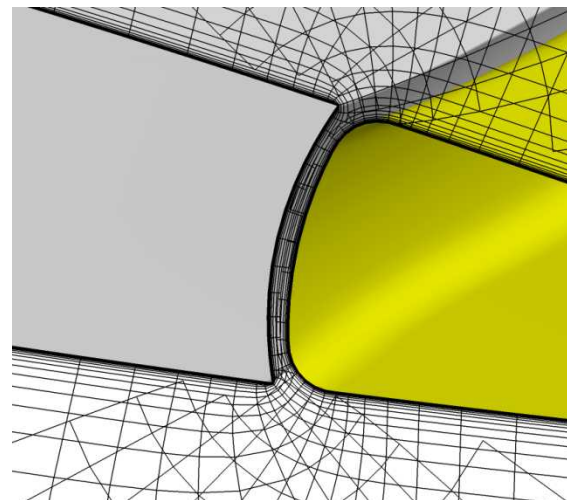
- Complex and expensive grid connectivity using object xrays
 - Tight tolerances to avoid collisions
 - Must be performed every step
 - Xrays do not handle disparate geometric fidelity very well
 - Poor donor compatibility possible
- Resolutions
 - Parallelized
 - Elasticized
 - Attention to details
 - Reduced memory
 - Cost reduced to < 20% flow solver step
 - Now in OVERFLOWv2.2



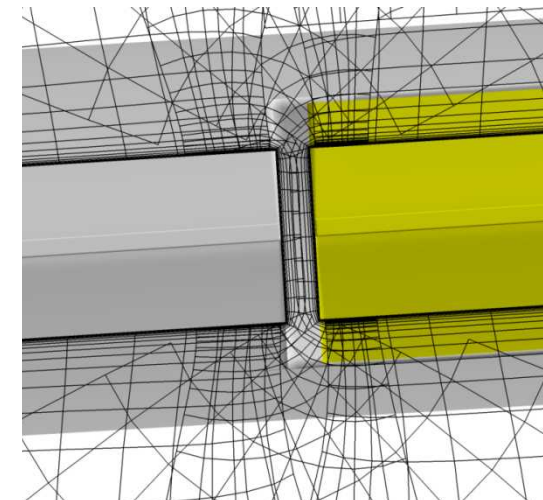
overset volume grids



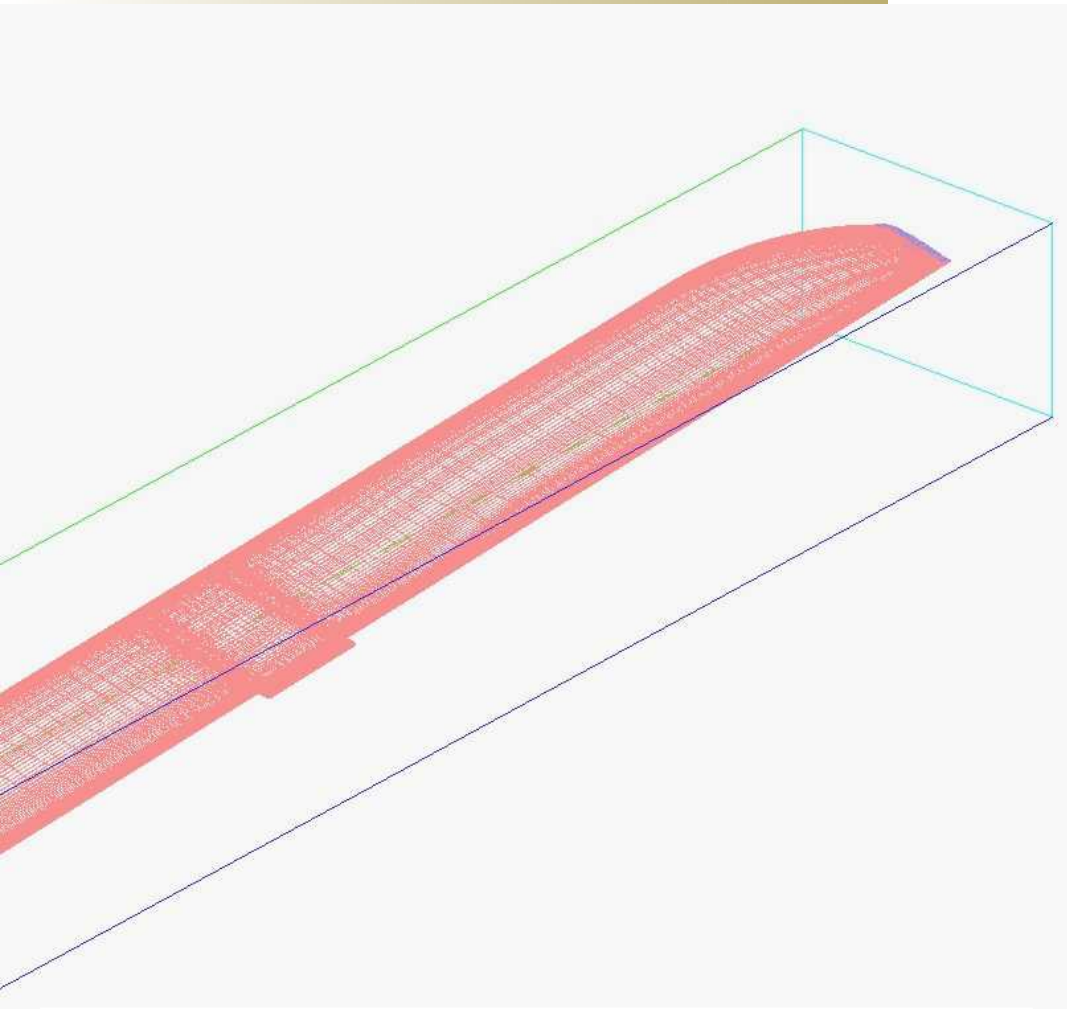
overset surface grids



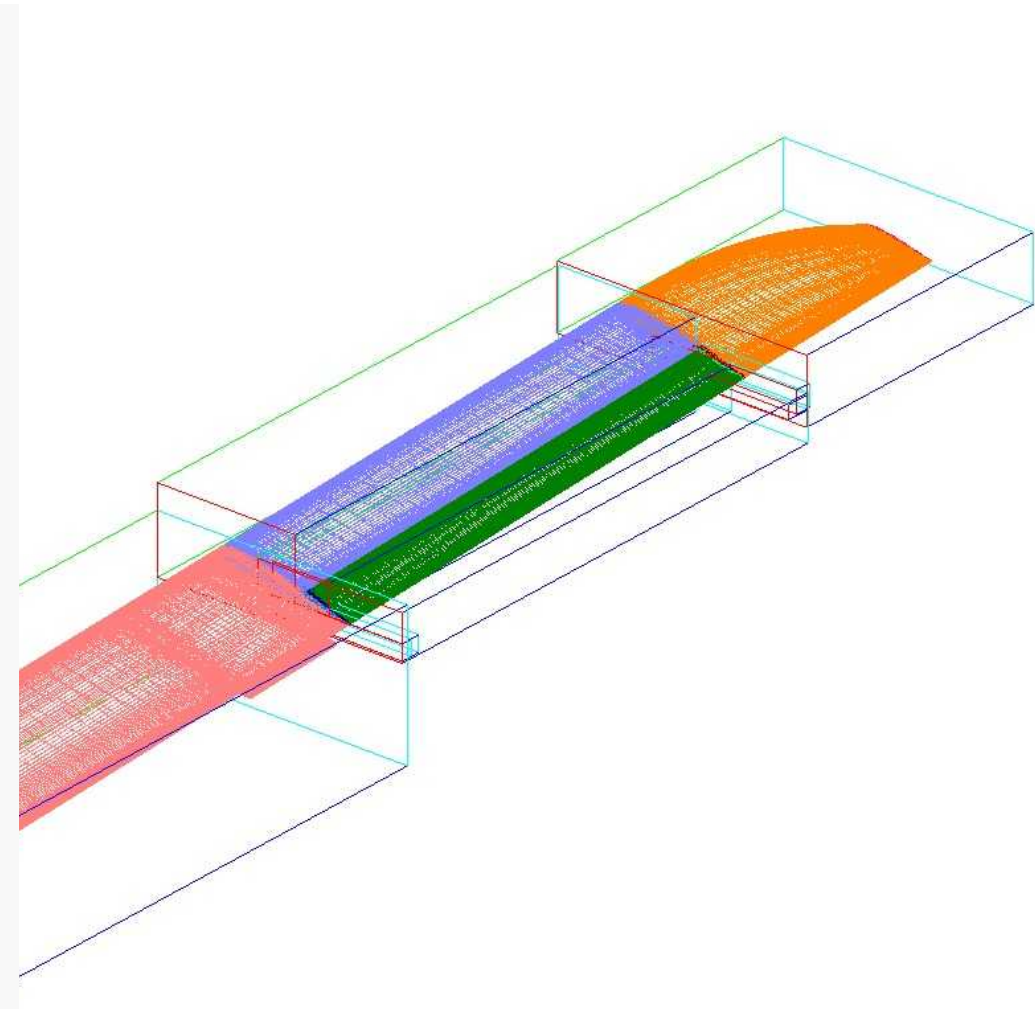
chordwise flap gap



spanwise flap gap (rear view)

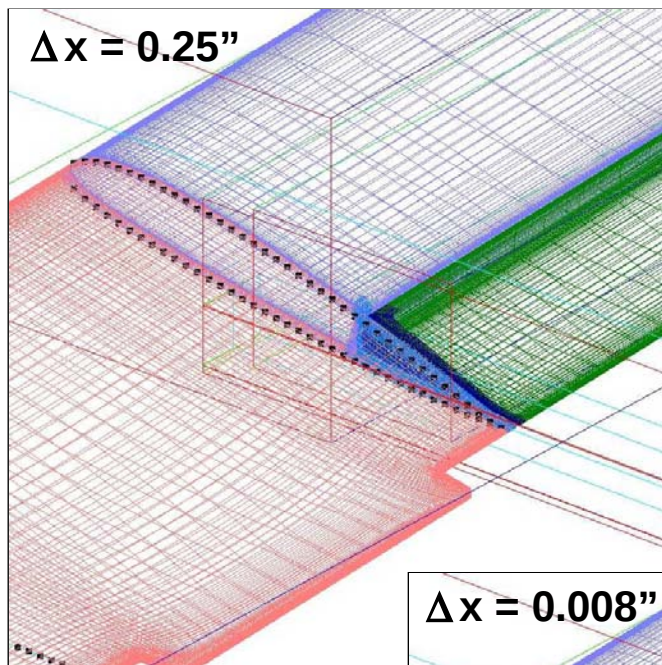


Single Blade - Single XRay
10MByte Xray file size

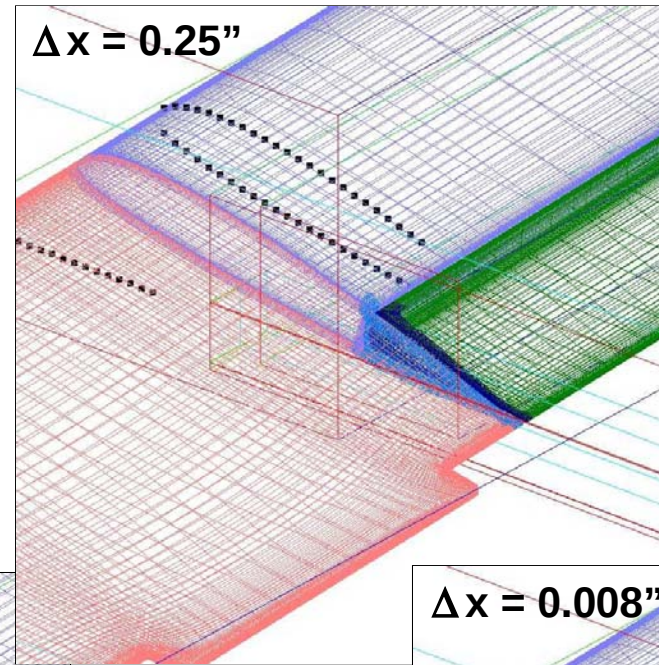


Blade and flap - 10 XRays
185MByte Xray file size

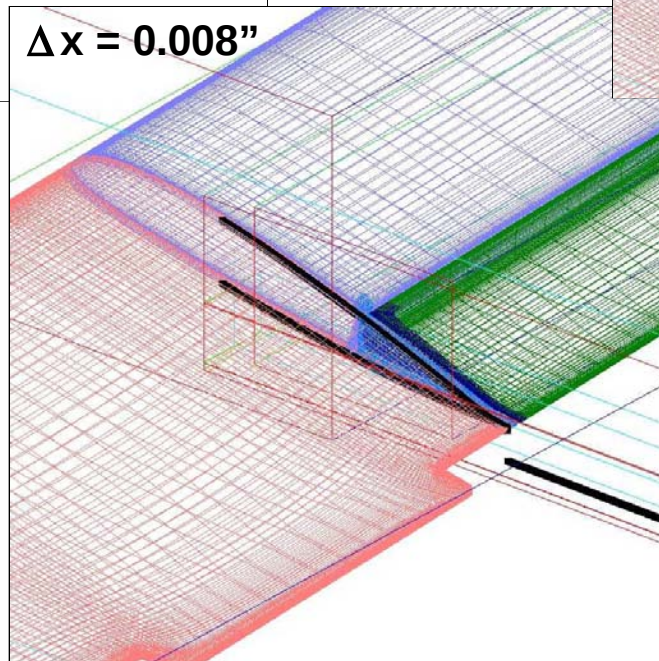
Coarse and fine grids have to use the same XRAYS



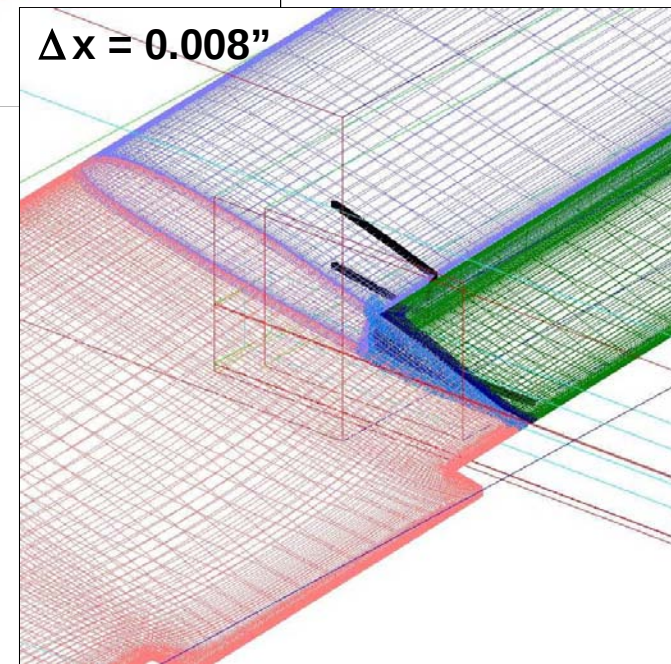
395 x 77



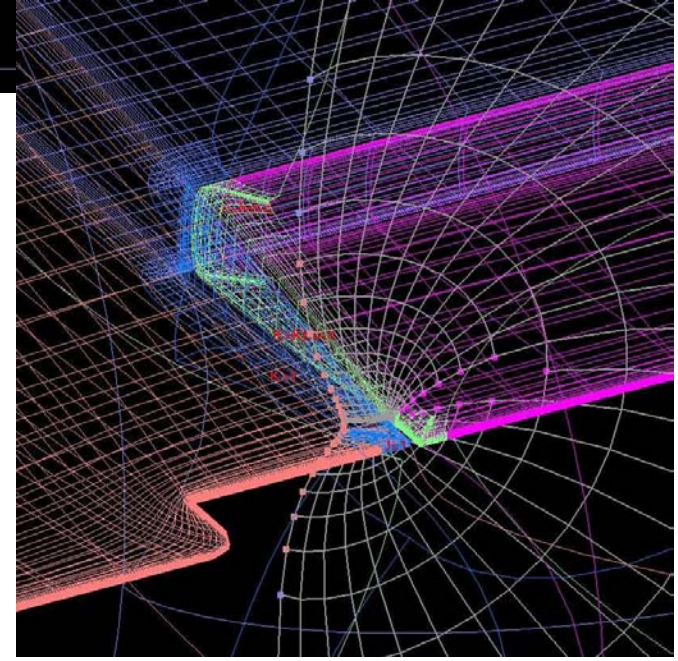
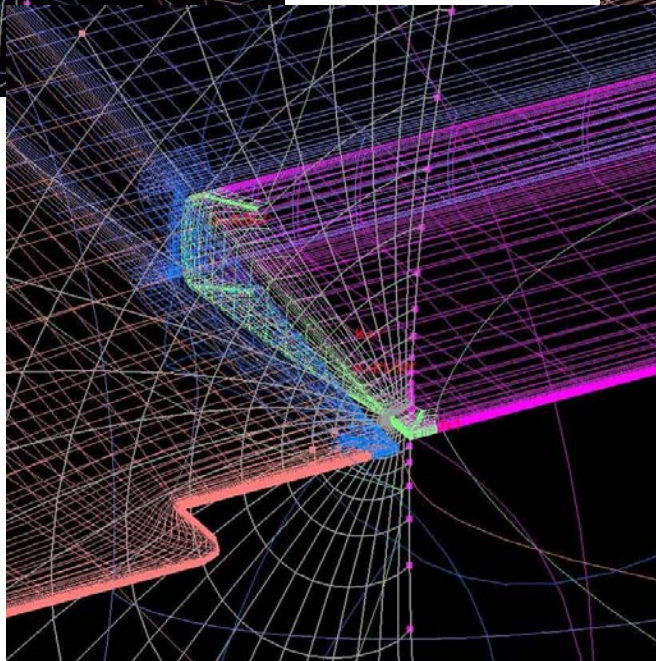
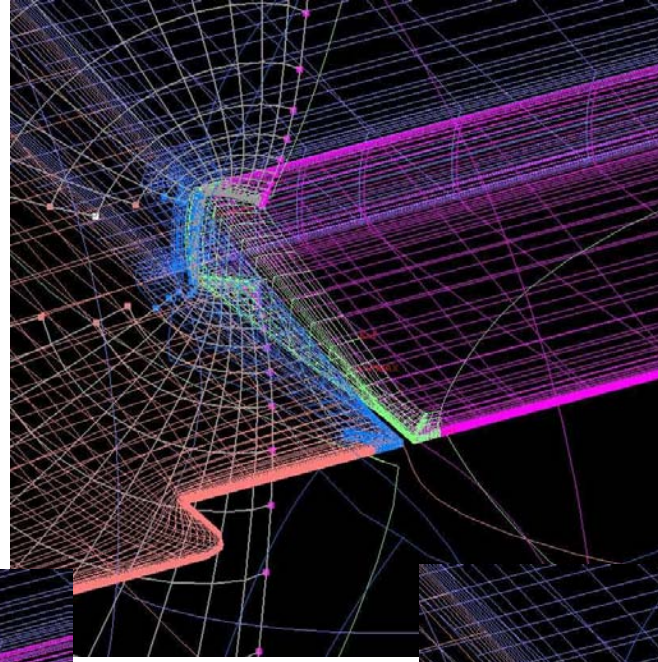
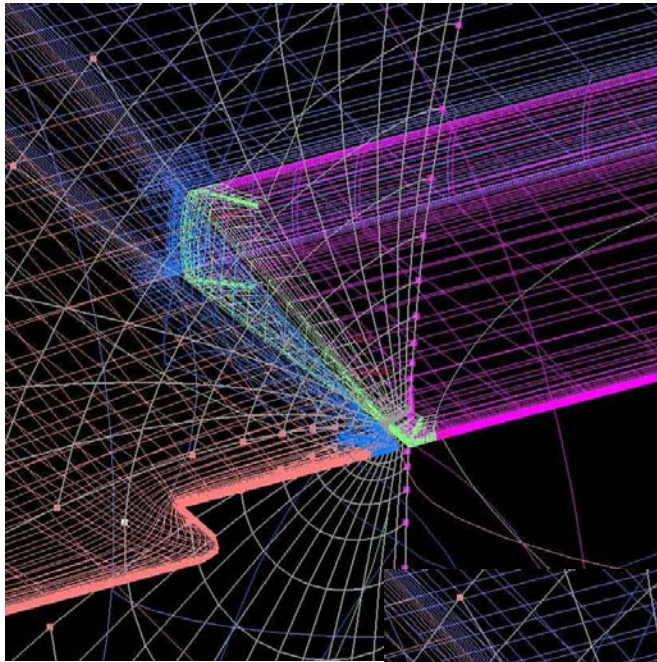
147 x 43



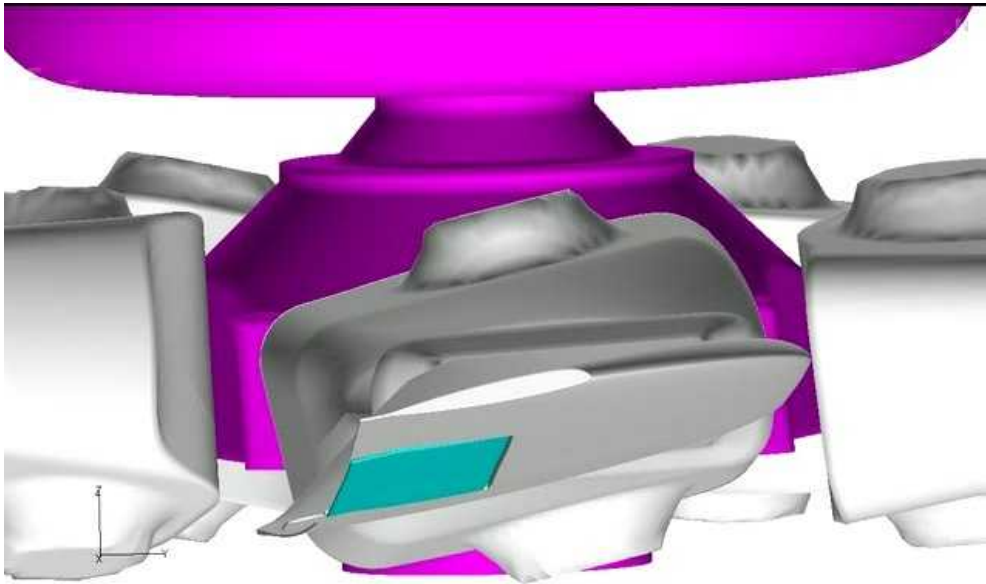
103 x 1376



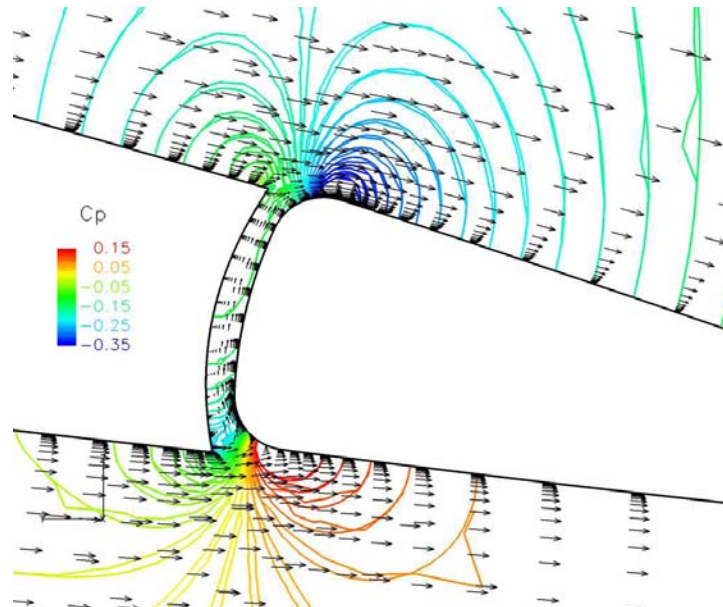
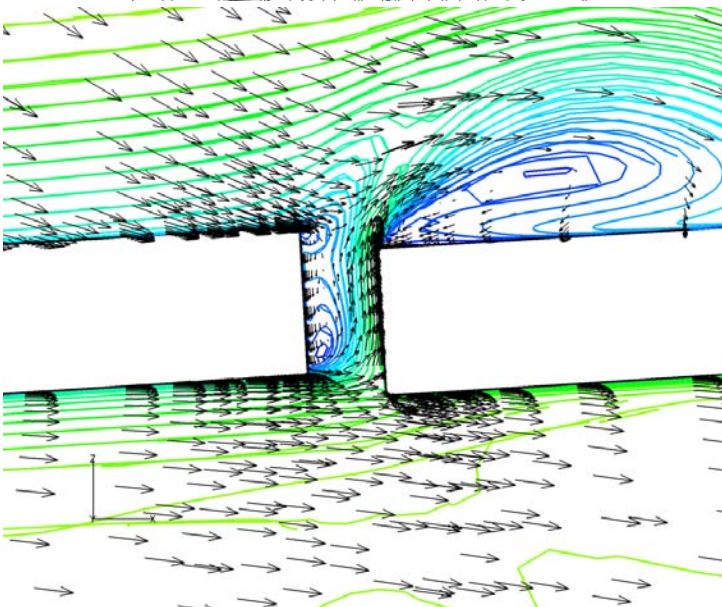
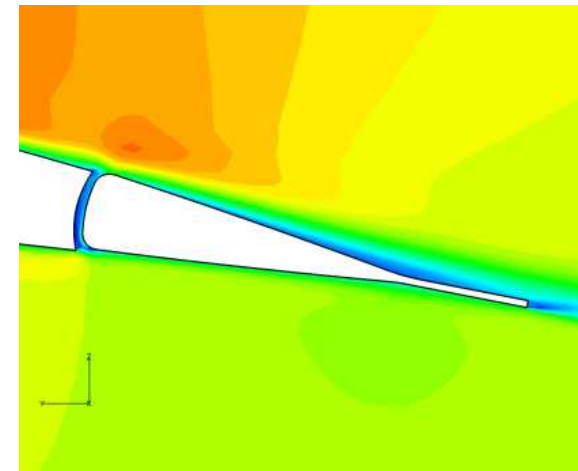
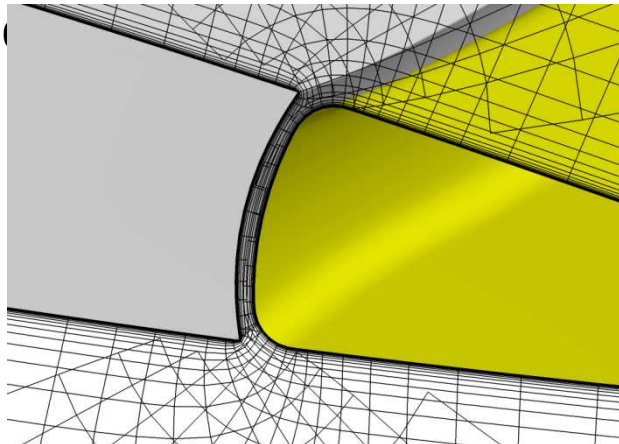
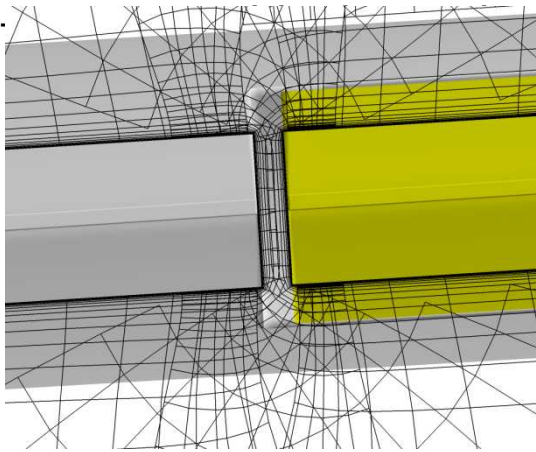
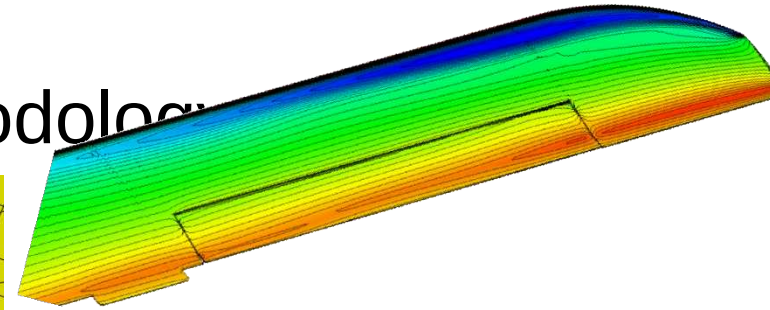
1831 x 221



- What could possibly go wrong!?



- Complex, 3D flow in flap gaps
- Major challenge for overset grid methodology



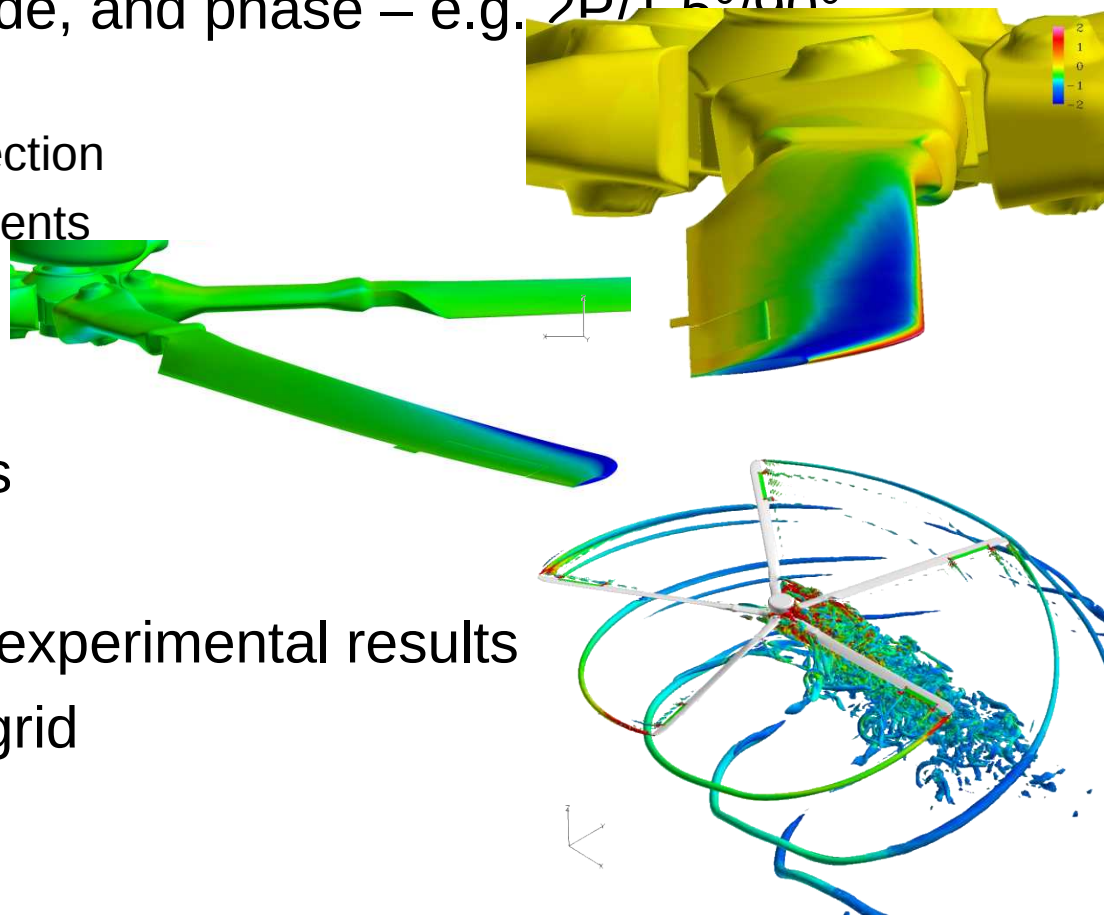
spanwise gap

chordwise gap

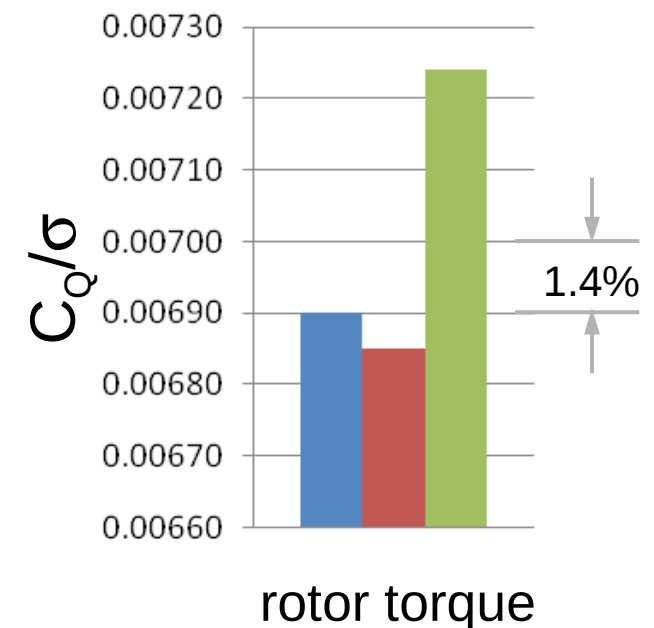
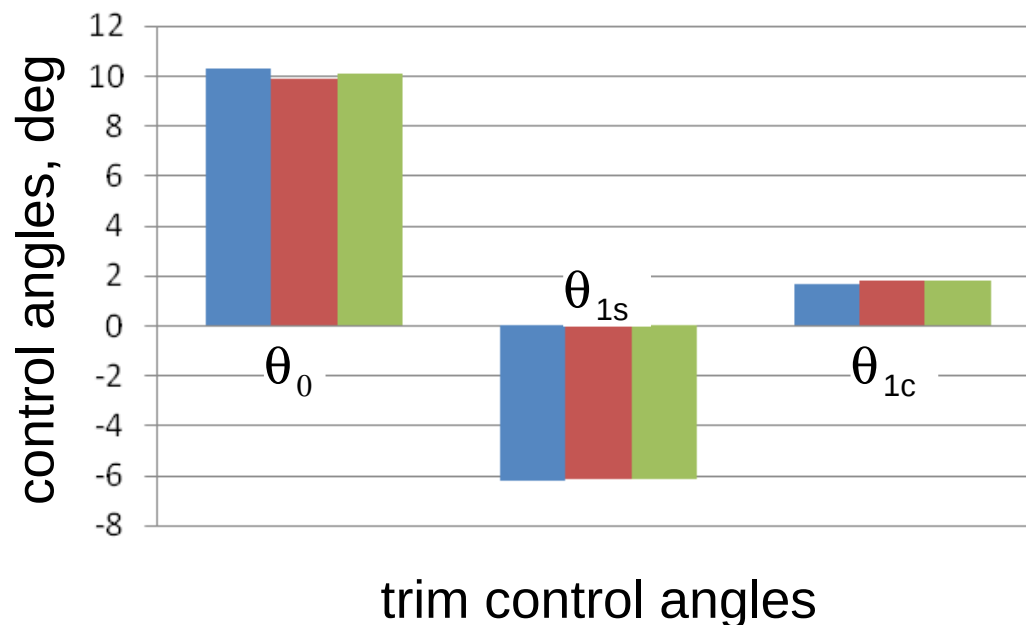
- Coupling every $2/5$ rev for 7 iterations (4 revs)
- Baseline coarse grid
 - 128 processors of a Cray XT5
 - 4.2 hours per rotor revolution
 - Coupled solution in ~16 hours
- Fine grid
 - 320 processors
 - 16 hours per rotor revolution



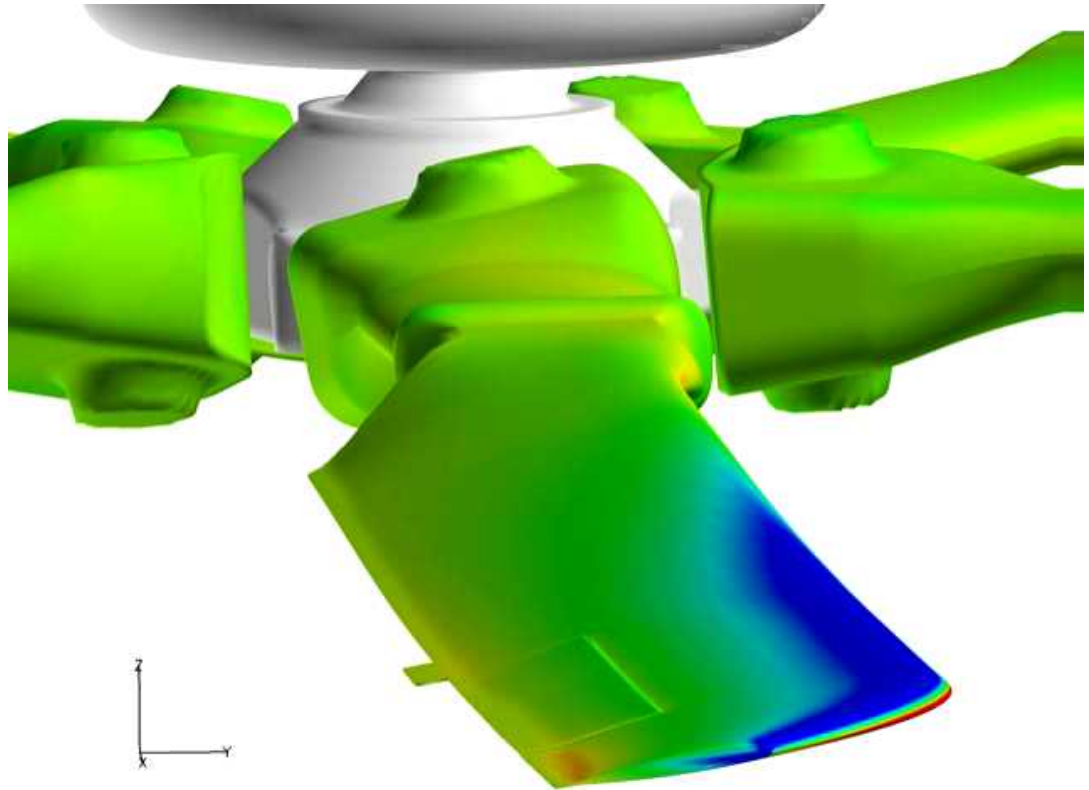
- Baseline flight conditions
 - $C_T/\sigma = 0.075$, 123 kts, 0.30 advance ratio, $\alpha_s = -9.1^\circ$ (nose down)
 - Trim conditions: thrust, zero flexbeam cyclic flapwise bending moment
 - Retrim at each flap input
 - Flap inputs: frequency, amplitude, and phase – e.g. 2P/1.5°/00°
 - Frequency: 0, 2, 3, 4, and 5/rev
 - Amplitude: nominal 1.5° flap deflection
 - Phase angle sweep in 30° increments
- Multidisciplinary investigations
 - Airloads and structural loads
 - Aerodynamics and flow physics
 - Performance
- Comparison with CAMRAD II and experimental results
- Most results use the coarse CFD grid



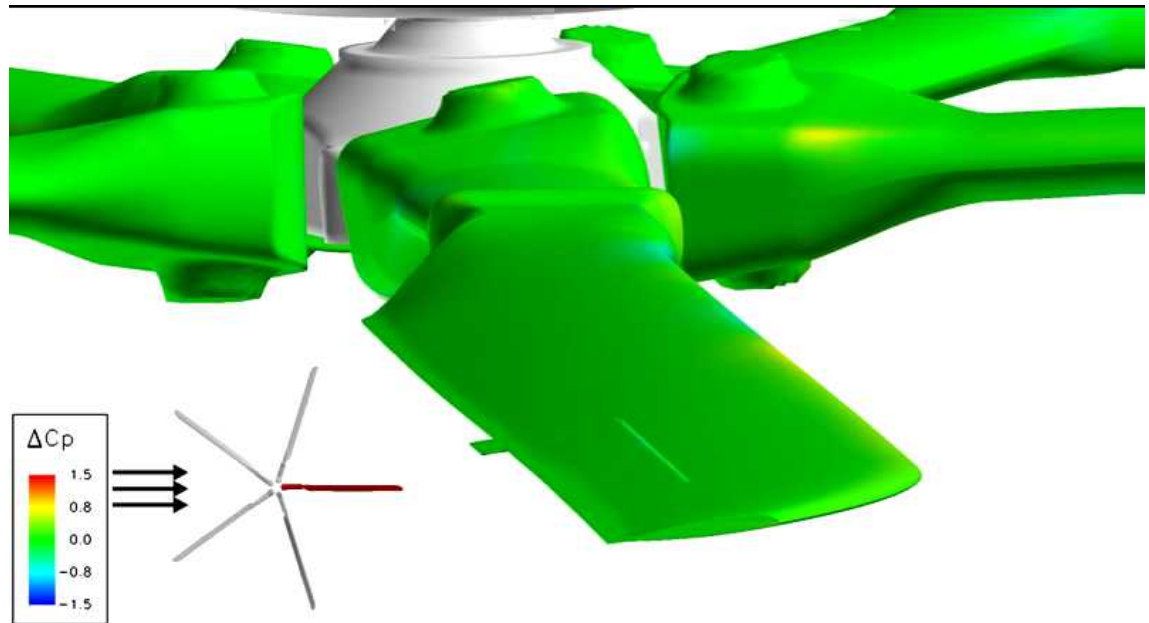
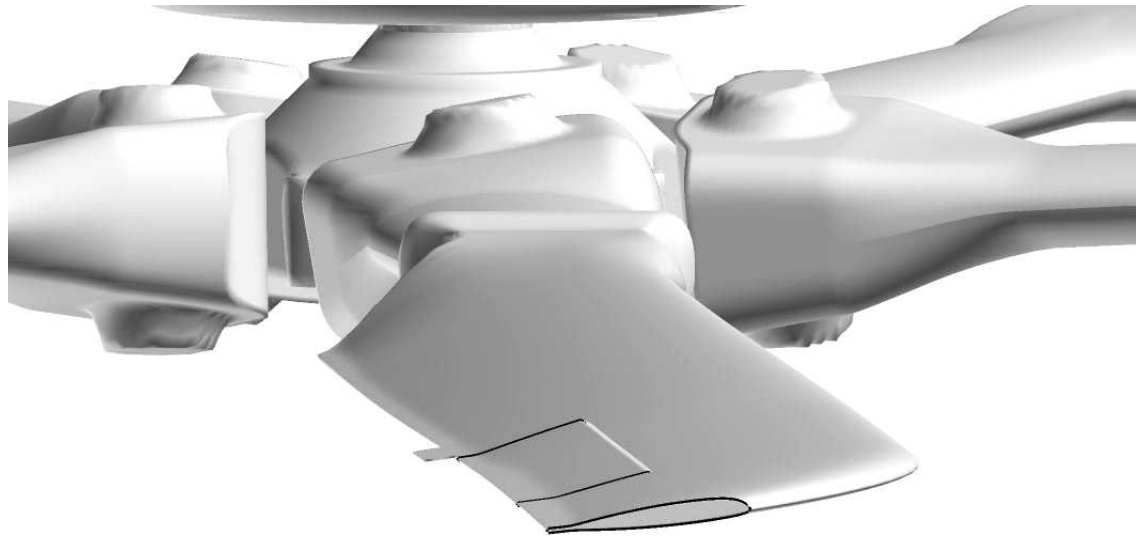
- No flap deflection SMART configuration
- Good agreement with test for pitch control angles and (fine grid) torque
- Consistent comparison with experimental force data buildup (including hub)



- Complex fluid-structure interactions
- Blade-fixed reference frame

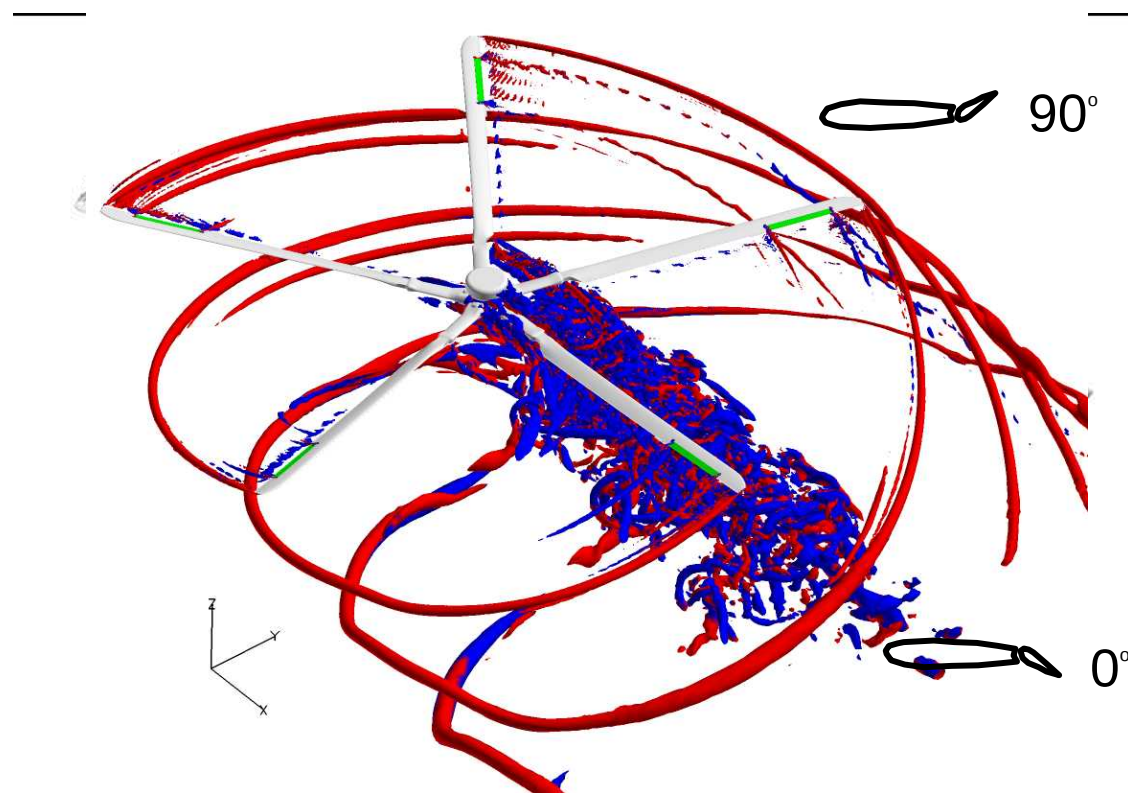


- Moment flap mechanism
- 5P/1.5°/180°
- Incremental motions (exaggerated) and pressures from the baseline



- Detailed wake visualization and interactions
 - Blade tip and flap end vortices
 - Hub wake
 - Super-vortex roll-up

2P/1.5°/90°



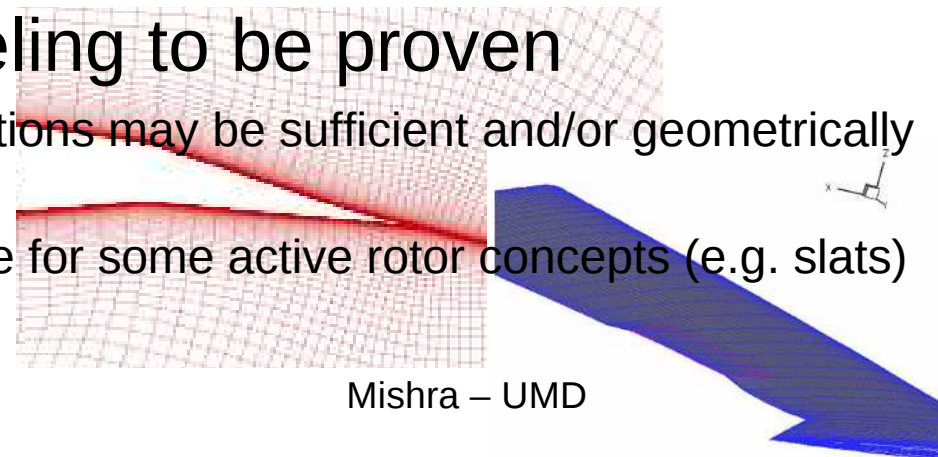
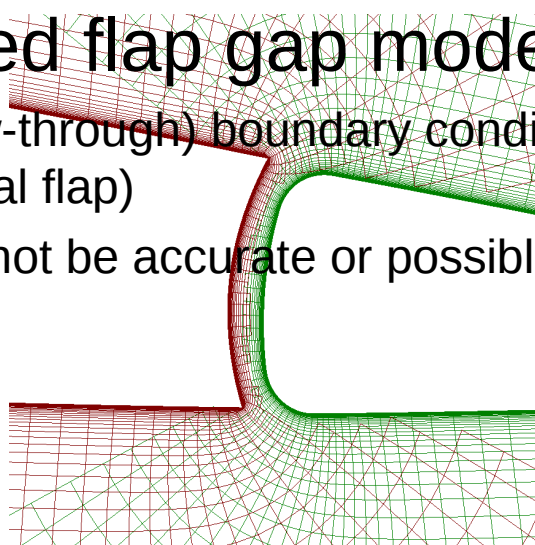
Q criterion

colored by sense of vorticity

- The SMART flapped rotor is a challenging configuration for current state-of-the-art CFD, CSD and CFD/CSD coupling tools
 - Considerable user expertise required
 - Need for automated and optimized CFD domain connectivity procedures
 - Need for CSD templates for complex configurations
- Modeling the flap gaps is a time consuming, detail-oriented task
 - Consistency in the fluid-structure interface required
- Need for detailed flap gap modeling to be proven
 - Simplified gap (flow-through) boundary conditions may be sufficient and/or geometrically realistic (e.g. integral flap)
 - Simplification may not be accurate or possible for some active rotor concepts (e.g. slats)



gap modeling



Mishra – UMD

integral flap, gap approximation

- NASA SRW Program, NASA (Boyd, Kottapalli, Warmbrodt, Johnson, Lau), Boeing (Straub), AFDD (Sim, Ruzicka), Georgia Tech (Bain), the SMART rotor team, the HPCMO HI-ARMS Institute, and Navy DSRC computer resources

