

Investigation of Hybrid Overset Grid-Based CFD Methods for Rotorcraft and Ship Airwake Flow Analysis

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Overview of the Presentation

- **Motivation**
 - Current issues
 - Contemporary strategies
 - New hybrid overset approach
- **Overview of VorTran-M**
- **CFD integration: Solver types**
 - Unstructured
 - Cartesian
 - Structured overset
- **CFD integration: Coupling strategy**
- **Information exchange: Cell intersection**
 - Vorticity-based coupling
- **Information exchange: Overset**
 - Velocity-based coupling
- **Ongoing and future work**
- **Conclusions**
- **Acknowledgements**

Motivation

- Reliable flow prediction is essential to the development of rotorcraft and the support of flight operations
- This requires accurate first-principles modeling of the rotor wake structure to predict blade airloads, fuselage loads and interactional aerodynamics

But ...

- Conventional grid-based CFD codes have high numerical diffusion of vorticity
- Lagrangian methods conserve vorticity, but have formulational limitations (i.e. core models, divergence, stability, cost)



AH-64 empennage evolution

Contemporary Strategies (focus on conventional CFD)

- Increase grid density
 - Costly
- Higher order methods
 - First order near steep gradients; complex; limited adaptation
- Modify Navier-Stokes equations to conserve angular momentum
 - More expensive; smearing of vorticity reduced, but still significant
- Modify error terms
 - Base convergence error on vorticity rather than primitive variables (2D)



RAH-66 empennage evolution

Hybrid grid-based solution

- **CFD code coupled to VorTran-M**
 - General interface exploiting modular/library construct of VorTran-M
- **Advantages**
 - Exploits features of both solvers (i.e. NS near to surfaces and VorTran-M in the wake)
 - Not constrained by configuration (i.e. rotorcraft only)
 - Solve the same fundamental equations
 - Enables automatic exploitation of both ongoing and future solver developments
- **Impact**
 - Improved capturing and preservation of complex wake structures (leading to reduced development costs)

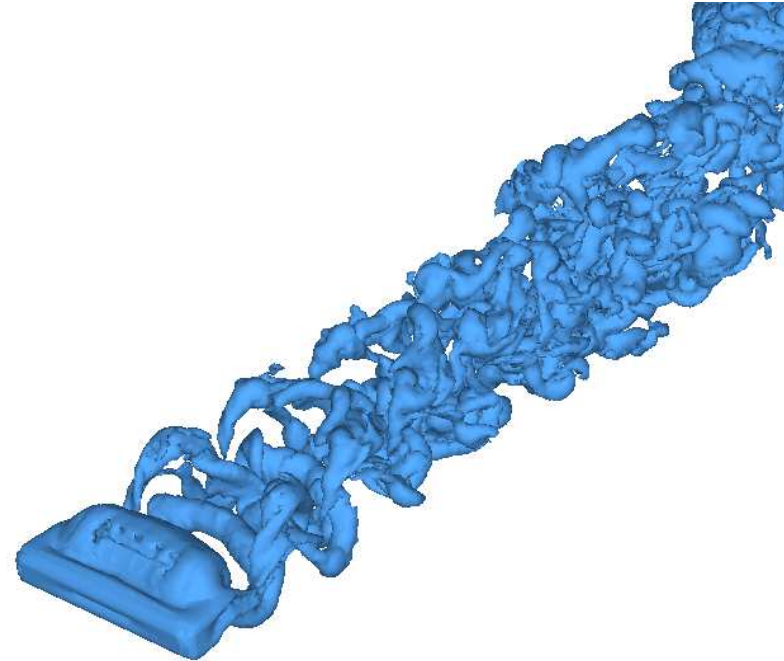


**X-2TD empennage
evolution**

Overview of VorTran-M

VorTran-M: Overview

- **Modularized and extended version of the CFD solver employed by Brown's VTM**
 - Module/software library
 - Adaptable interface source code
 - Whitehouse et al, Overset Grid Symposium 2006
 - Whitehouse et al, AHS Forum 2007
 - Keller et al, I/ITSEC 2007
 - Whitehouse and Tadghighi, AHS Aeromechanics Conference, 2010
 - Whitehouse et al, AHS Forum 2010
- **General coupling interface strategy**
 - Supports multiple “inner solver” formulations and grid constructs
 - Supports multiple simultaneous solver types



CFD/VorTran-M prediction of the wake behind a wing at 90° angle of attack

VorTran-M: Flow solver

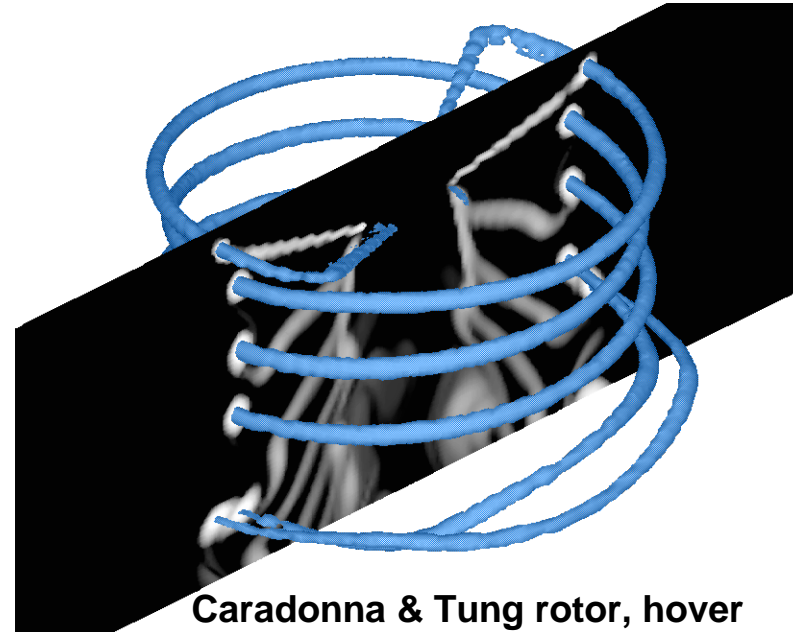
- Solves the incompressible Navier Stokes equations (vorticity-velocity form)

$$\frac{\partial}{\partial t} \omega + u \cdot \nabla \omega - \omega \cdot \nabla u = \nu \nabla^2 \omega + S$$

$$\nabla^2 v = -\nabla \times \omega$$

using a variant of Toro's WAF scheme

- Cell centered adaptive grid scheme
- Fast Biot-Savart / Poisson solvers
- Over 10 years of continued development
- Extension to compressible flow has been formulated



Caradonna & Tung rotor, hover
800,000 cells. 50 cells/R, 6 cells/c



Harris rotor, $\mu=0.04$

370,000 cells, 40 cells/R, 2.8 cells/c

CFD Integration: Solver Types

Target host solvers

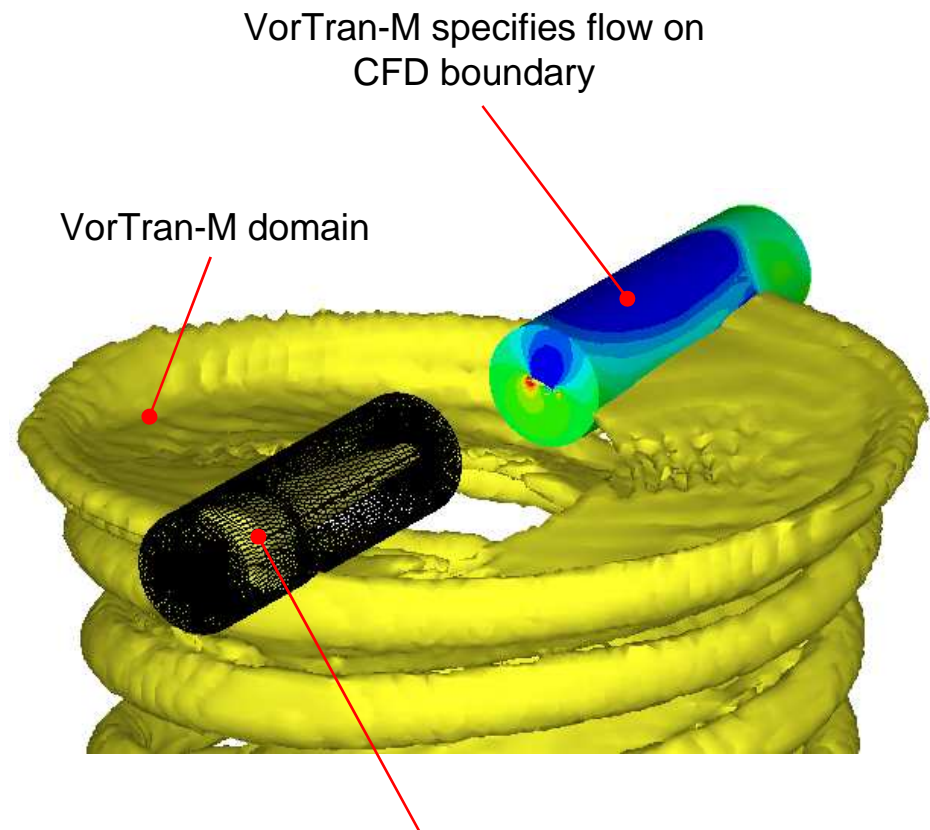
- **Goal is to interface with a wide variety of solver and grid types**
 - RANS/Euler
 - Structured
 - Unstructured
 - Moving and deforming grids
 - Overset
- **Solvers investigated**
 - RSA3D
 - Rotor Stator Aeroelastic analysis in 3D
 - Developed for NASA GRC by CDI
 - Multiple 3D unstructured deforming moving grids (sliding interface)
 - Tightly coupled nonlinear FE solver
 - AIAA-1994-0415, AIAA-1994-2269, Whitehouse *et al* AHS Forum 2007
- **Solvers investigated (cont'd)**
 - CGE
 - Cartesian Grid Euler solver
 - Developed by CDI for design apps.
 - 3D adaptive Cartesian grid
 - Support for imperfect geometries
 - AIAA-1994-0415, AIAA-1994-2269, Keller *et al* IITSEC 2007
 - OVERFLOW
 - NASA structured overset grid RANS solver
 - AIAA-1999-3302, AIAA-2009-3988 etc
 - FUN3D
 - NASA unstructured grid RANS solver
 - NASA TM-4295, AIAA-2009-1360 etc

CFD Integration: Coupling Strategy

CFD Integration: Coupling Strategy

Overview of Coupling Strategy

- CFD solver calculates near-body flow field
- CFD solver sets VorTran-M solution in suitably defined overlap region
- Evaluation of Biot-Savart law in VorTran-M accounts for all contributions:
 - Vorticity evolved in VorTran-M
 - Flow field transferred from CFD solver
- VorTran-M solution feeds into CFD domain at outer boundaries
- Minimizing extent of CFD domain allows higher resolution within the domain and less numerical diffusion



CFD calculates flow field to initialize
the VorTran-M solution

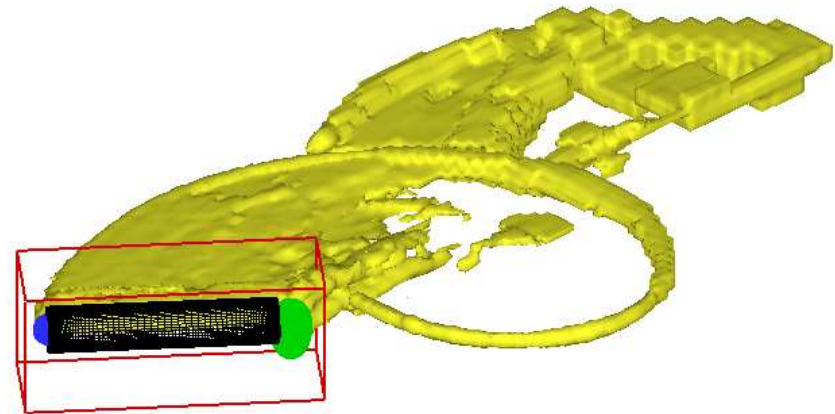
Schematic of coupling strategy

Information Exchange: Cell Intersection

Information Exchange: Cell Intersection

Vorticity-based coupling

- Vorticity in CFD domain calculated by finite differencing
- Intersection between CFD cells and VorTran-M cells performed
 - Establish relationship between each CFD cell and corresponding VorTran-M cell
- Volume weighted vorticity inserted into VorTran-M
- If inviscid, then include the vorticity on the surface (i.e. bound vorticity)
- CFD outer BCs set by VorTran-M
- Implemented in
 - RSA3D (unstructured)
 - CGE (Cartesian grid)
 - OVERFLOW 2.1 (overset structured)

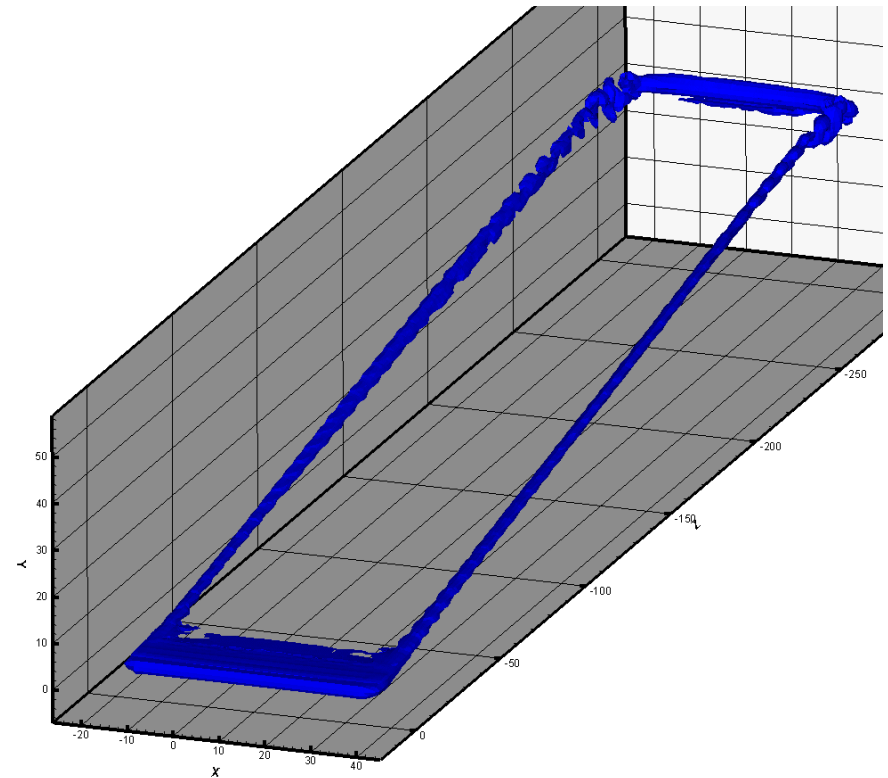


Iso-surface of vorticity magnitude for single bladed rotor in forward flight (OVERFLOW/VorTran-M)

Information Exchange: Cell Intersection (cont'd)

RSA3D

- Formal intersection between RSA3D's tetrahedral and VorTran-M's cubic cells
- Impulsively started wing at 8°
 - Inviscid
 - NACA 0012
 - Aspect Ratio = 8.8
 - $M=0.2$
 - 128 points around airfoil (270K tets.)
 - 1.5c upstream, 2.5c downstream
 - VorTran-M cell size = 0.18c
- Predicted lift coefficient on coarse grid to within 1.1% of inviscid theory



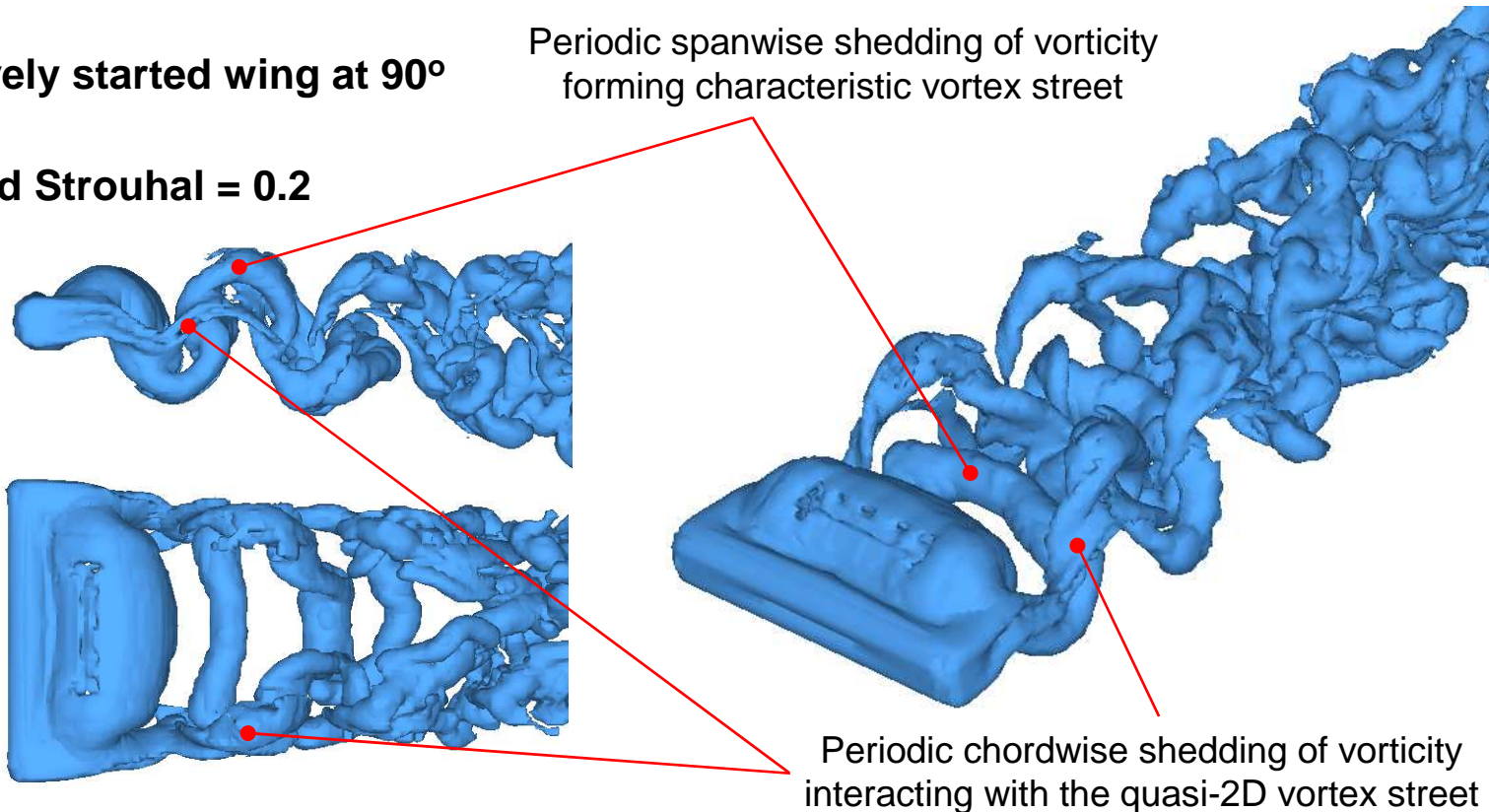
Perspective view of the developing wake structure for the impulsively started wing

Information Exchange: Cell Intersection (cont'd)

RSA3D (cont'd)

- Impulsively started wing at 90°
- Predicted Strouhal = 0.2

Periodic spanwise shedding of vorticity
forming characteristic vortex street

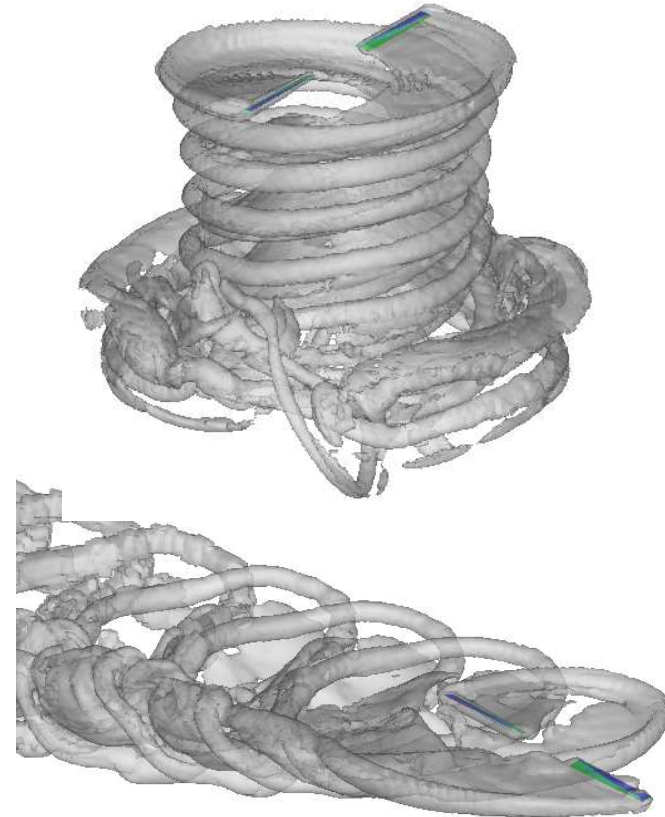


Iso-surface of vorticity magnitude showing near
wake behind a wing at 90° angle of attack

Information Exchange: Cell Intersection (cont'd)

RSA3D (cont'd)

- **Untrimmed 2-bladed rotor**
 - VR12
 - 10° twist
 - 72K tets. per blade
 - Open root section (i.e. no root vortex)
 - Blades are disjoint
- **Demonstrated overset-moving grid capability of the interface**

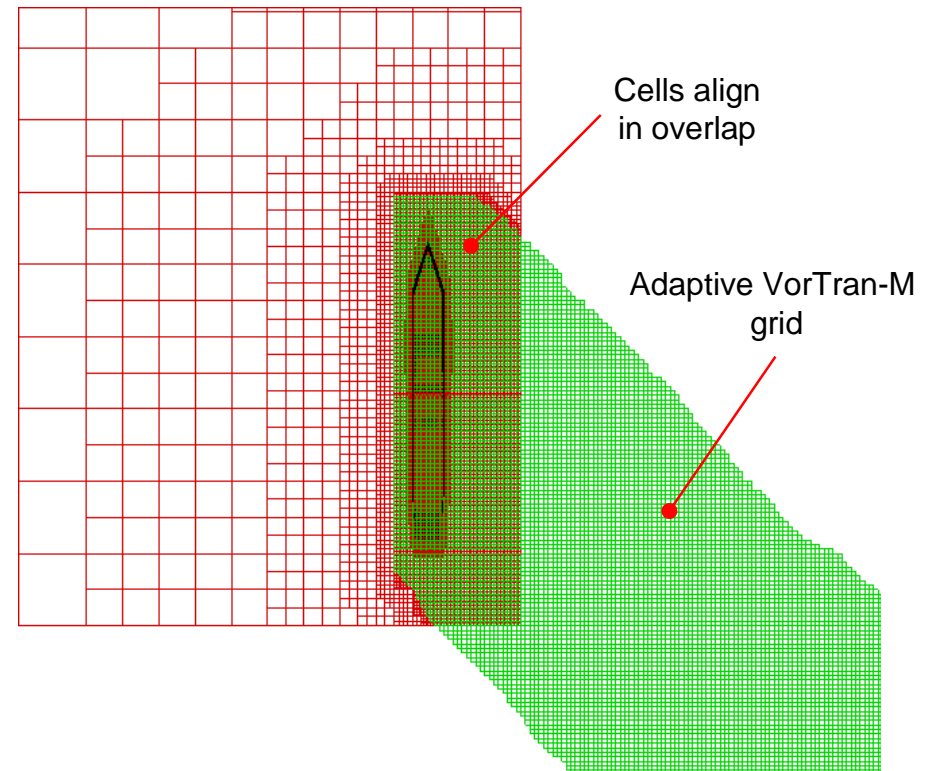


**RSA3D/VorTran-M rotor wake predictions:
two bladed untrimmed rotor in slow speed ascent
(upper) and two bladed untrimmed rotor in
forward flight (lower)**

Information Exchange: Cell Intersection (cont'd)

CGE

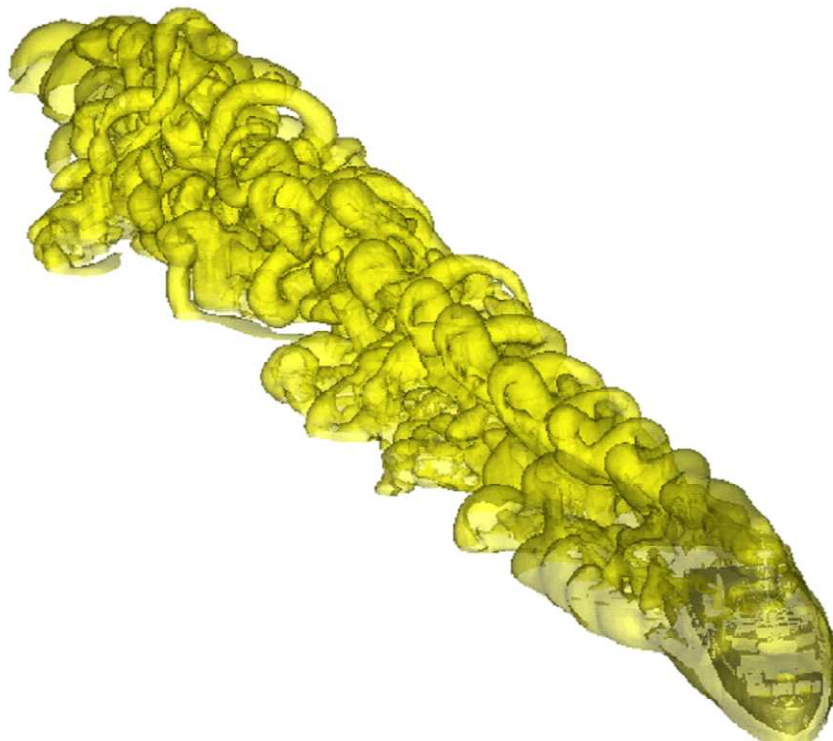
- **Formal intersection between Cartesian grid and VorTran-M cells**
 - Trivial since tight control placed over Cartesian grid
- **Ship airwake calculations**
 - Undertaken during development of ship airwake database for CAE (MH-60R/SH-60B TOFT)
 - >192 ship/wind combinations
 - First commercially-generated ship airwake database
- **NACA 0015**
 - Lift within 0.65% of experiment
 - Tip vortex position within 1%
 - Tip vortex core within 1.6% at 4c



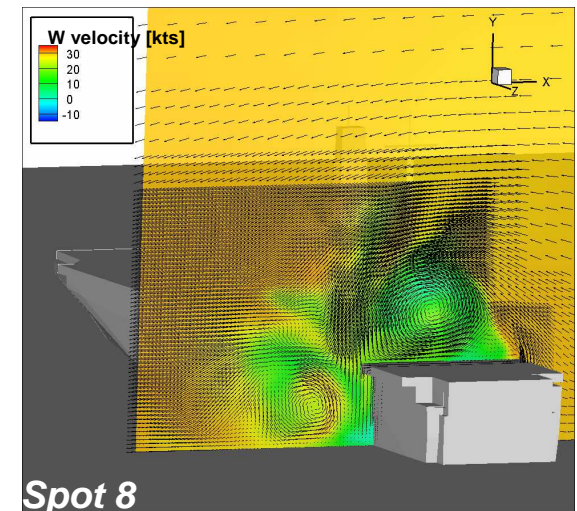
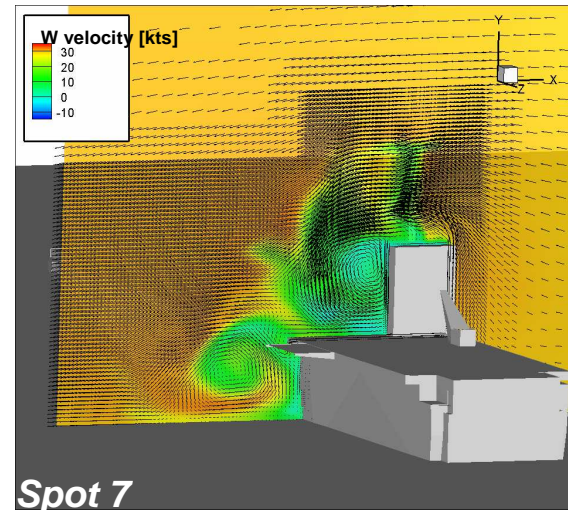
CGE/VorTran-M grid intersection

Information Exchange: Cell Intersection (cont'd)

CGE (cont'd)



LPD-4 ship airwake

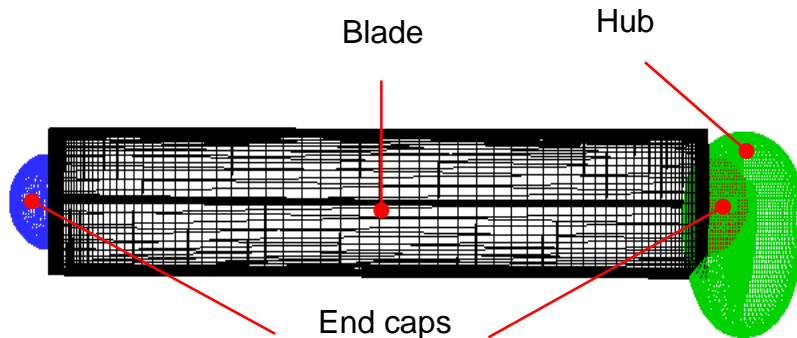


Velocity contours and vectors of
an LHA airwake in a crosswind

Information Exchange: Cell Intersection (cont'd)

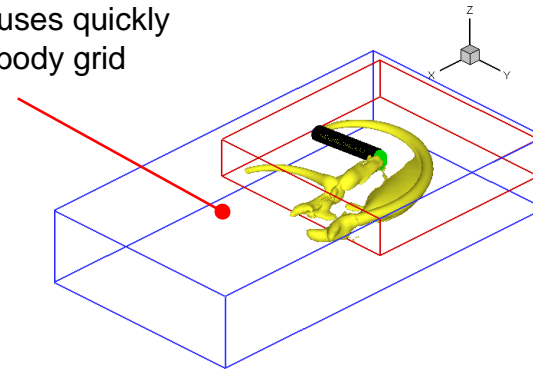
OVERFLOW (2.1ab)

- **Vorticity inserted at cell centroid**
 - Tight control placed on grid surrounding rotor (aligns with VorTran-M)
- **1-bladed rotor in forward flight**
 - 5 overlapping near-body grids
 - OVERFLOW/VorTran-M and OVERFLOW calculations on similar grids



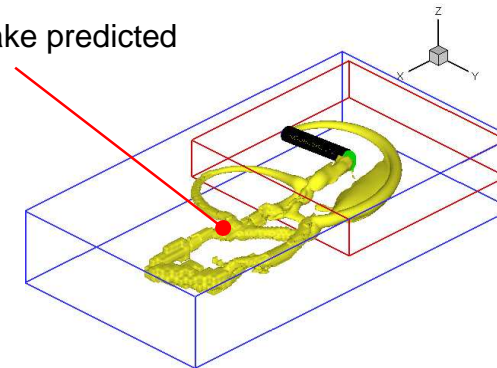
Blade and hub grids

Wake diffuses quickly
in off-body grid



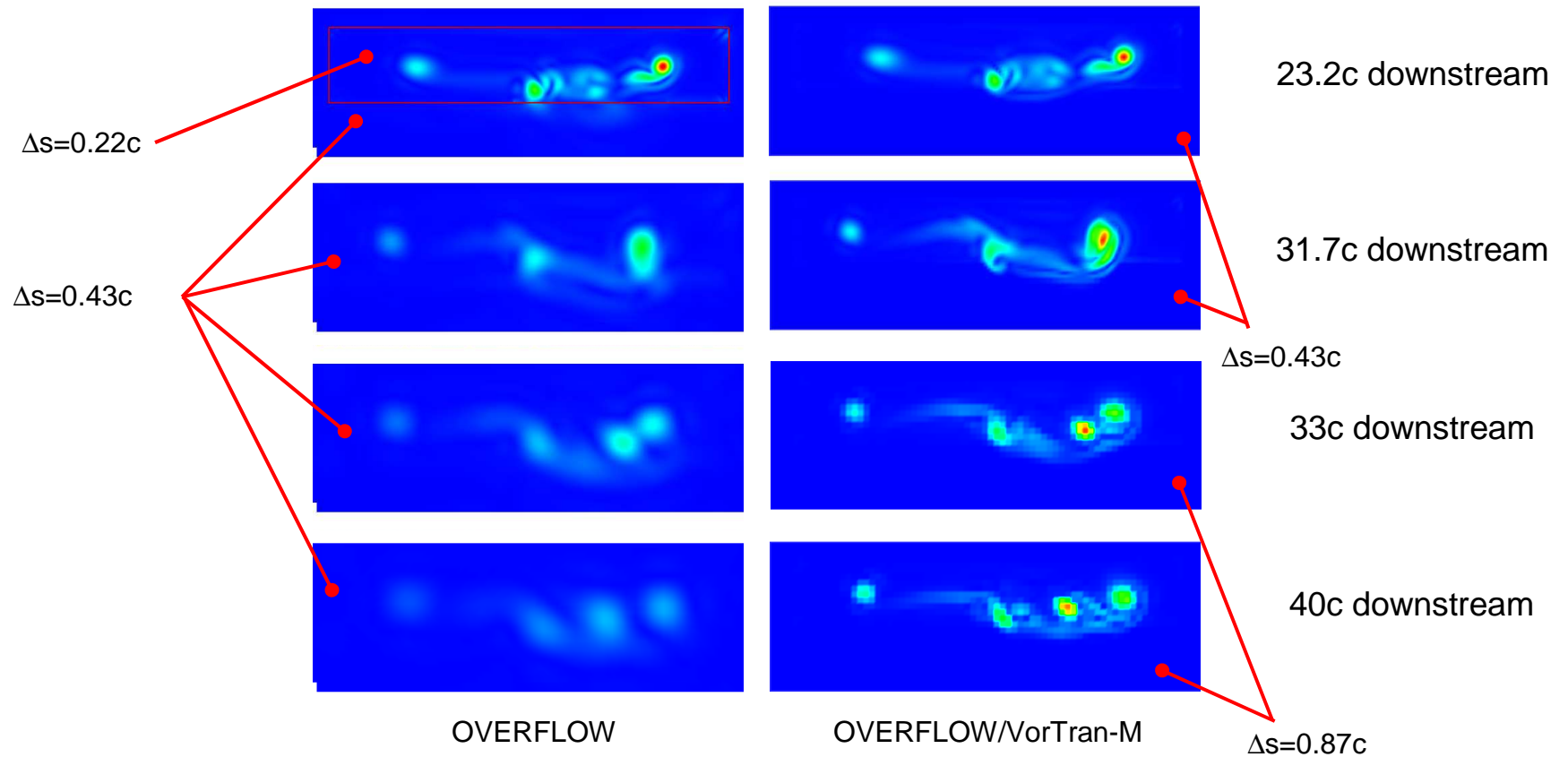
Iso-surface of vorticity magnitude OVERFLOW

Entire wake predicted



Iso-surface of vorticity magnitude
OVERFLOW/VorTran-M

Information Exchange: Cell Intersection (cont'd)

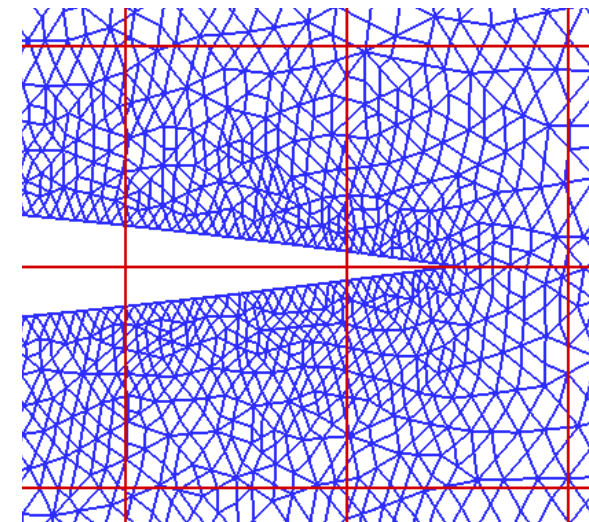
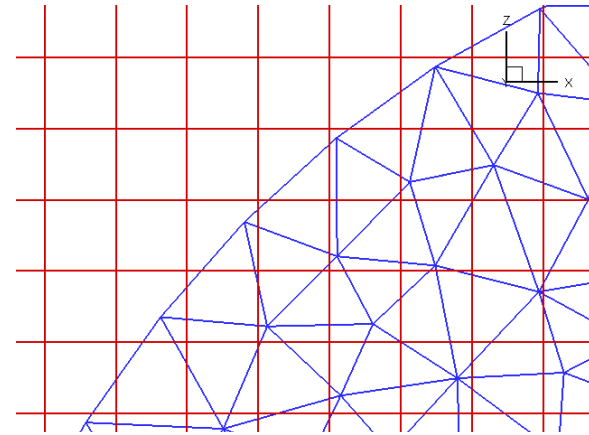


Slices through the grid for a 1-bladed rotor in
forward flight

Information Exchange: Cell Intersection (cont'd)

Lessons learned

- Cell intersection exhibits positive results for a variety of solvers and applications
- In general, requires formal intersection
 - Complicated
 - Costly
 - Invasive
- For structured and Cartesian grid-based approaches, intersection costs can be reduced
 - Tight control must be placed on grid
- Requires vorticity to be calculated in every overlapping CFD cell
 - Costly

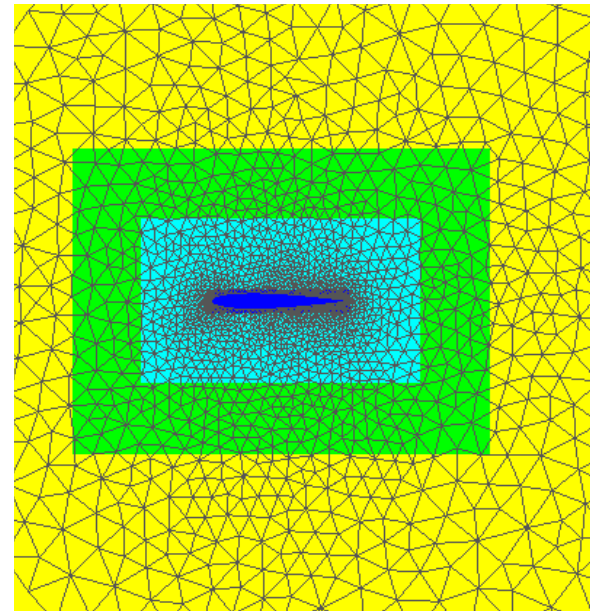


Intersection of unstructured (blue) and VorTran-M grids (red) at left and center

Information Exchange: Overset

Velocity-based coupling

- CFD solution (velocity) calculated at overlapping VorTran-M cell corners
- Overlap/buffer regions can be determined entirely in terms of VorTran-M cells
 - IBLANK information
 - Simple surface-based cell marking
- Velocity passed to VorTran-M
- CFD BCs set on outer boundary
- Implemented in
 - OVERFLOW 2.1 (overset structured)
 - FUN3D (unstructured)

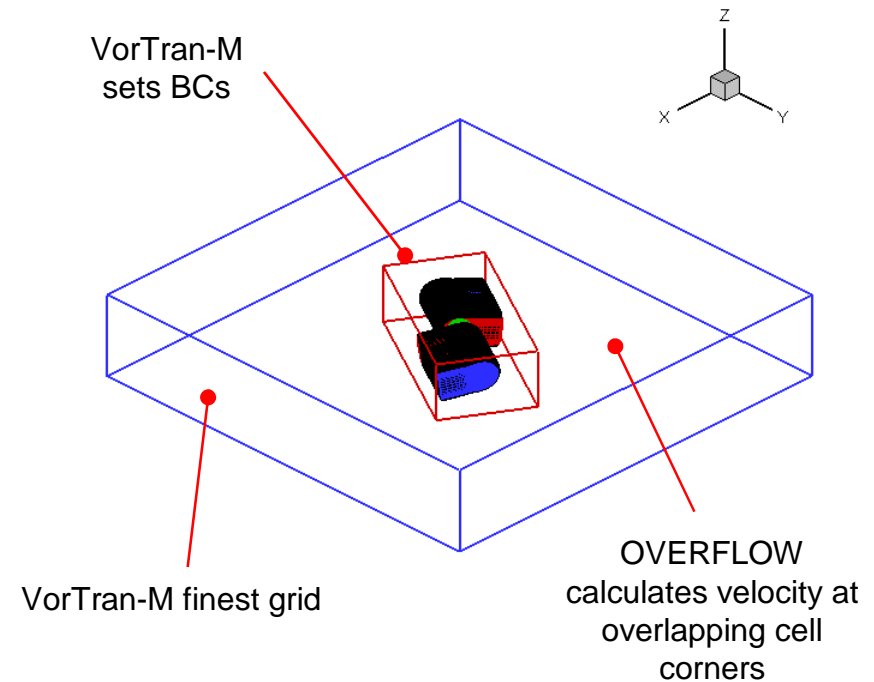


Sample surface-based cell marking

Information Exchange: Overset (cont'd)

OVERFLOW (2.1ab)

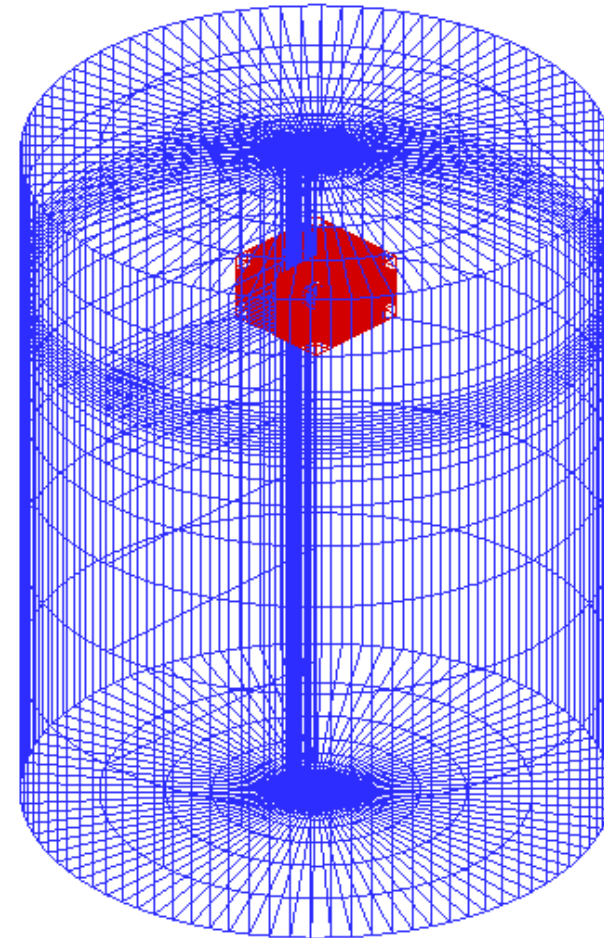
- **2-bladed Caradonna and Tung rotor**
 - 8° collective
 - 1250 RPM
- **OVERFLOW/VorTran-M grids**
 - “Engineering scale” and strategy
 - 8 overlapping near-body grids
 - 2 rotor blades, each with
 - Main blade
 - 2 End caps
 - Body of revolution hub
 - 1 surrounding grid (cubic cells, rotates with blades)
 - ~6.4 Million OVERFLOW nodes
 - ~800,000 VorTran-M cells



**Schematic of OVERFLOW/VorTran-M
velocity-based coupling**

OVERFLOW (2.1ab)

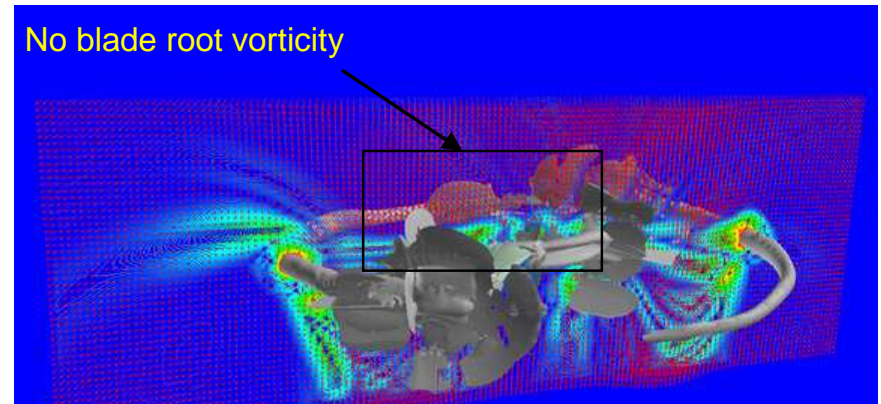
- **OVERFLOW (coarse grid)**
 - “Engineering scale” and strategy
 - Same NBGs as OVERFLOW/VorTran-M
 - Automatic off body grid generation (factor of 2 scaling)
 - ~19.8 Million Nodes
- **OVERFLOW (fine grid)**
 - Same NBGs as OVERFLOW/VorTran-M
 - Background rotating O-grid
 - Source BCs
 - ~24 Million Nodes



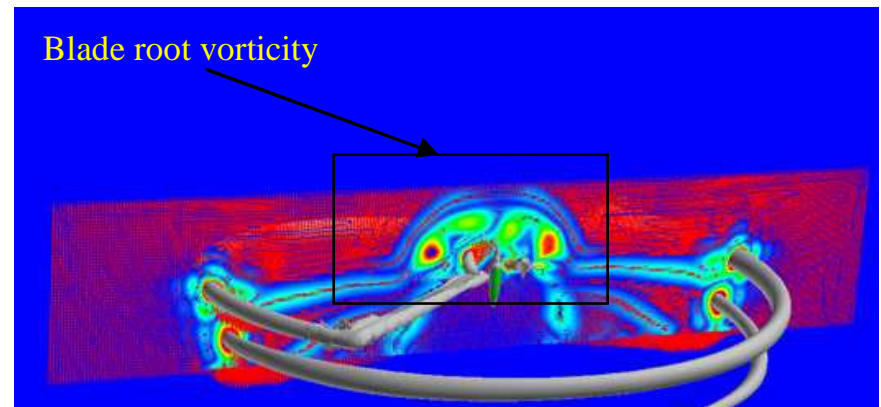
Fine OVERFLOW grid system

OVERFLOW (2.1ab) (cont'd)

- **Comparisons**
 - General wake prediction
 - Loading
 - Tip vortex trajectory
- **Trim**
 - Experiment
 - $C_T=0.046$
 - OVERFLOW (coarse grid)
 - $C_T=0.0432$
 - 94% of experimental value
 - OVERFLOW (fine grid)
 - $C_T=0.0492$
 - 102% of experimental value
 - OVERFLOW/VorTran-M
 - $C_T=0.0458$
 - 99.6% of experimental value



OVERFLOW (coarse grid) predictions of the wake near to the rotor

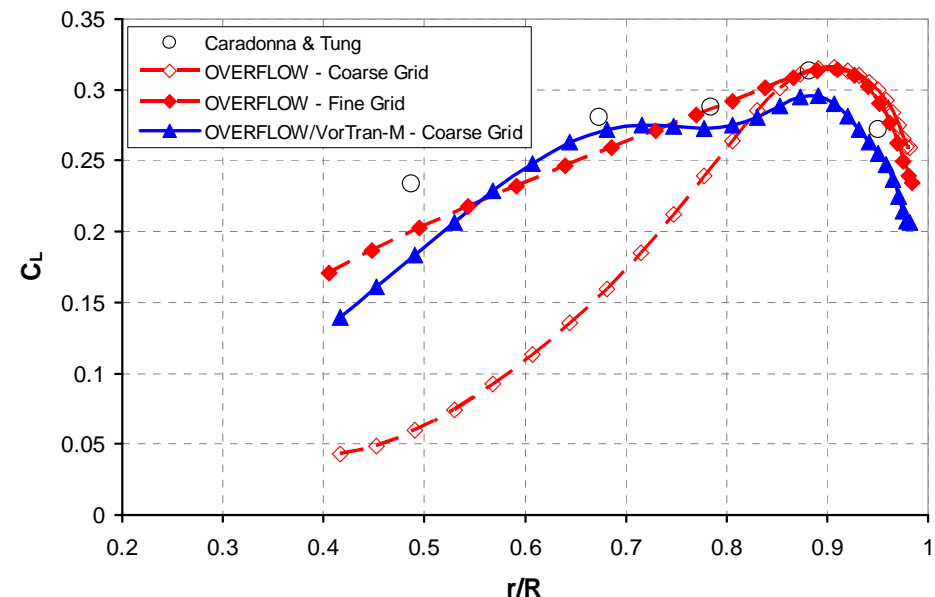


OVERFLOW/VorTran-M predictions of the wake near to the rotor

Information Exchange: Overset (cont'd)

OVERFLOW (2.1ab) (cont'd)

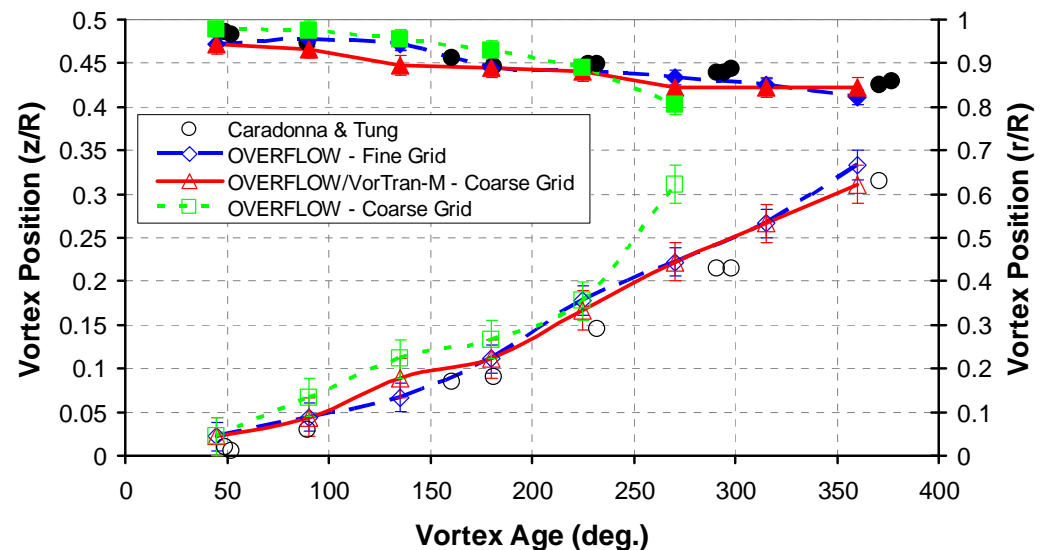
- **OVERFLOW (coarse grid)**
 - Very little inboard loading
 - Overprediction at tip
- **OVERFLOW (fine grid)**
 - More accurate inboard loading
 - Slight overprediction at tip
- **OVERFLOW/VorTran-M**
 - Slight underprediction of tip loading
 - More accurate mid-span loading
 - Underprediction of inboard loading



Comparison of measured and predicted spanwise loading

OVERFLOW (2.1ab) (cont'd)

- **OVERFLOW (coarse grid)**
 - Tip vortex diffuses significantly after $\sim 135^\circ$, identification is impossible after $\sim 270^\circ$
 - Tip vortex is outboard and lower than measurements
 - Significant increase in descent rate after $\sim 180^\circ$
- **OVERFLOW (fine grid) and OVERFLOW/VorTran-M**
 - Vertical and radial tip vortex position predicted correctly
 - Radial contraction asymptote predicted correctly

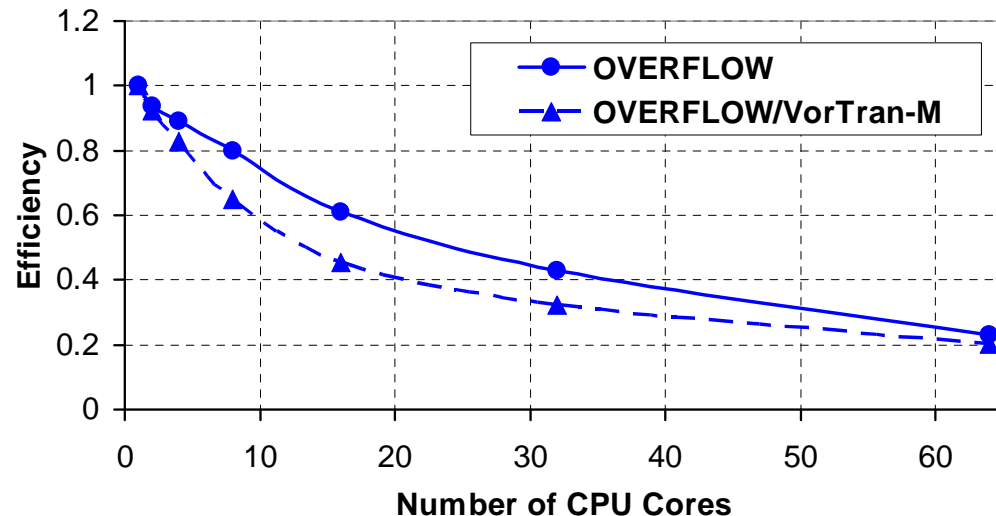
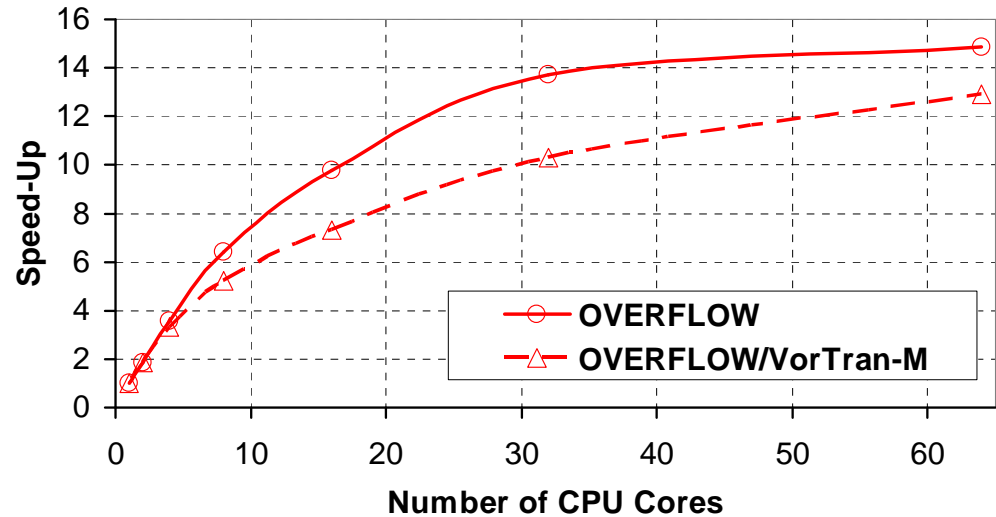


Comparison of measured and predicted
spanwise loading

Information Exchange: Overset (cont'd)

OVERFLOW (2.1ab) (cont'd)

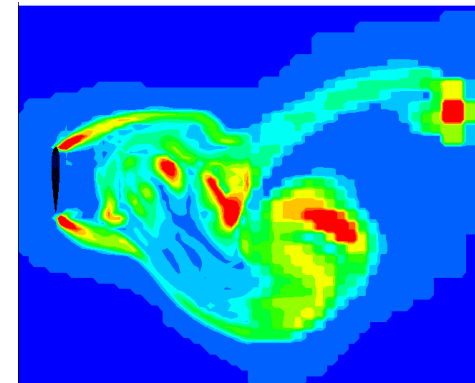
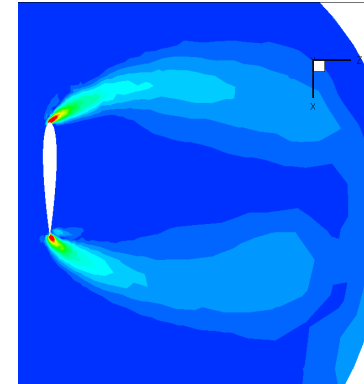
- **Porting**
 - Shared memory (SGI Altix)
 - Distributed memory (MJM and other beowulf clusters)
 - Assorted compilers (Intel, Portland, GNU)
- **Scalability**
 - Tested on 72 core Microway distributed memory cluster using both OpenMPI and MPICH



Information Exchange: Overset (cont'd)

FUN3D

- **Impulsively started wing at 90°**
 - NACA 0012
 - Aspect Ratio = 8.8
 - $M=0.2$
 - 128 points around airfoil (270K tets.)
 - 1.5c upstream, 2.5c downstream
- **Viscous**
 - Spalart-Allmaras turbulence model
- **Additional ongoing demonstrations presented in Quon E. “Not Your Father’s Hybrid Code: Advancements in CFD-Based Hybrid Methods for a New Millennium”**

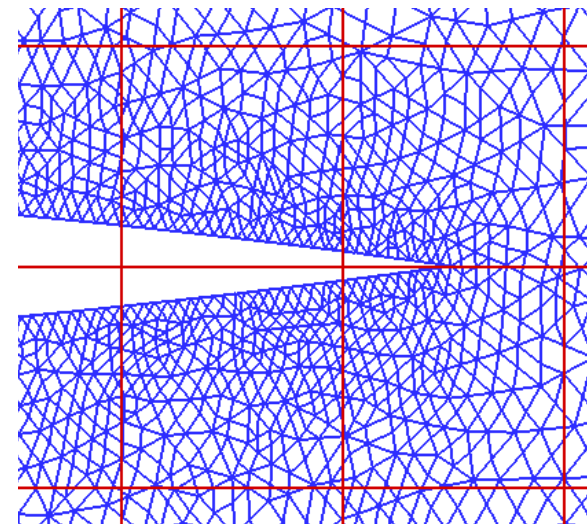
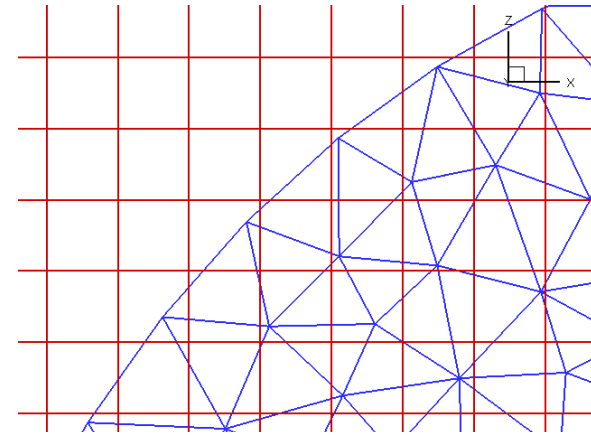


Mid-plane vorticity magnitude predicted by the FUN3D/VorTran-M coupled simulation for the NACA0012 wing at 90° angle of attack

Information Exchange: Overset (cont'd)

Lessons learned

- **Overset velocity-based approach addresses many of the limitations of the insertion method**
 - Intersection operations replaced with velocity interpolation procedures
 - Simpler and already available in many solvers
 - Less information exchanged between host solver and Module
 - Amount of information exchanged now determined by VorTran-M cell size, not local CFD cell size
 - Requires that the CFD solver can preserve the vorticity sufficiently in the overlap region



Intersection of unstructured (blue) and VorTran-M grids (red) at left and center

Conclusions

- **Demonstrated five CFD/VorTran-M couplings using two difference interfacing strategies**
 - Unstructured (RSA3D and FUN3D)
 - Cartesian (CGE)
 - Structured overset (OVERFLOW)
- **Demonstrated improved predictions**
 - Fixed wing
 - Bluff body
 - Isolated rotors
- **Observed improved efficiency**
 - Fewer cells required for comparable fidelity predictions
 - Simple mesh constructs and BC appear to be adequate for problems investigated to date

Acknowledgements

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Presentation End